UNIVERSAL MECHANISM 9



User`s manual



Simulation of dynamics of flexible bodies

UM module for simulation of flexible bodies allows including finite-element models of flexible bodies into Universal Mechanism models. Issues of importing finite-element models, their interaction with other bodies as well as simulation of dynamics of hybrid systems are considered.

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11. Simulation of dynamics of flexible bodies using UM FEM

11.1. Introduction

UM FEM module is a set of software tools that are built-in **UM Input** and **UM Simulation** programs. The module gives a user a possibility to introduce flexible bodies under large displacements into a model of mechanical system. Flexible displacements are supposed to be small in the body-fixed frame of reference and could be described in terms of linear finite-element analysis (FEA). Introducing flexible bodies into a model of mechanical system is used for creating the more detailed models and obtaining more accurate results of simulation.

In some cases modeling the system with the help of rigid bodies only is too rough approximation of a real system. Then some bodies of the model should be considered as flexible, for example, car body and chassis of transport machines. Using flexible bodies to obtain more accurate solution (coordinates, accelerations) and widen its spectrum that might be important in some cases, for example, for analysis of vibrations and durability of machines.

UM FEM needs that **UM Subsystems** module is also being installed on your computer. As well as it is necessary that a FEA preprocessor and solver are available on your computer. The present **UM FEM** version supports import from following FEA software:

- **ANSYS** software version **5.5** and higher;
- MSC.NASTRAN 2005, MSC.NASTRAN 2007, MSC MD NASTRAN 2010, MSC.NASTRAN 2012;
- NX NASTRAN 8.0, NX NASTRAN 9.0.
- ABAQUS 6.10-1.

It supposes that the user has at least basic skills in finite element analysis and using FE software, as well as has an idea of modal approach.

In this section some basic information concerning methods of simulation of flexible bodies in **UM FEM** is presented.

Mathematical model of a flexible body is based on using the following methods:

- subsystem technique,
- floating frame of reference method,
- finite-element method,
- Craig-Bampton method.

Every flexible body is considered as a separate subsystem that is why assembly of composite¹ model is similar to assembly of multibody model. Before assembly the preliminarily step of preparing the necessary data of FE-model of flexible bodies should take place. Flexible bodies/subsystems can interact with any other rigid or flexible bodies with the help of joints and force elements.

¹ Composite or hybrid model includes both rigid and flexible bodies

11.1.1. Kinematics

Kinematics of flexible bodies is described with the help of so called *floating frame of reference CS1*. Kinematical formulas are noted in this *floating frame of reference*. Position of certain point *K* of the flexible body in the global CS0 is defined as follows (Figure 11.1):

$$\mathbf{r}_{k}^{0} = \mathbf{r}_{01}^{0} + \mathbf{A}_{01}(\mathbf{\rho}_{k}^{1} + \mathbf{d}_{k}^{1}), \qquad (11.1)$$

where \mathbf{r}_{01} is radius vector of the origin of CS1 in CS0, \mathbf{A}_{01} is transformation matrix, $\mathbf{\rho}_k$ is radius vector of point *K* of undistorted flexible body in CS1, vector \mathbf{d}_k presents elastic displacements of the point, superscript denotes the coordinate system in which vectors are given.



Figure 11.1. Floating frame of reference

Elastic properties of the flexible bodies relatively to the CS1 are described with the help of finite-element method. The present **UM FEM** version supports import of data about flexible bodies from external FE software products.

Small elastic displacements are presented as a sum H of possible modes/shapes of flexible body:

$$\mathbf{x} = \sum_{j=1}^{H} \mathbf{h}_j w_j = \mathbf{H} \mathbf{w},\tag{11.2}$$

where **x** is nodal degrees of freedom of the flexible body, h_j is the possible mode, w_j is the *modal* coordinate that describes flexible displacements correspond to mode *j*. The matrix **H** is called *modal* matrix.

According to the Craig-Bampton method the *modal* matrix is formed as a combination of *eigenmodes* and *static modes*. The method consists of four steps.

- 1. Choice of *interface (boundary)* nodes of a finite-element scheme.
- 2. Successive calculation of *static* modes. Static modes are static shapes obtained by given each boundary d.o.f. a unit displacement while holding all other boundary d.o.f. fixed.
- 3. Calculation of *eigenmodes* while holding all *interface* nodes fixed;
- 4. Calculation of the mass matrix and the stiffness matrix, orthonormalization of the eigenmodes and static modes.

The short description of the each step is given below.

Choice of interface nodes. Flexible body/subsystem interacts with other bodies of the model via joints and force elements. It is recommended that every attachment point should be situated

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in the node of finite-element mesh. Very these nodes, where joints and force elements are attached to, should be chosen as *interface* nodes. Such an approach helps to create joint constrains correctly and quite accurate describe flexible displacements that determine force in force element.

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It is necessary to choose *interface* nodes so as during calculation of each *static* mode the immobility of the subsystem was guaranteed.

Calculation of static modes. The number of static modes is equal to number of d.o.f. in *in-terface* nodes. During this procedure *interface* nodes are held fixed and static modes are obtained by given each interface d.o.f. a unit displacement/rotation.

Calculation of eigenmodes. Eigenmodes of flexible body are obtained from the solving the generalized eigenproblem:

$$(\mathbf{C} - \lambda \mathbf{M})\mathbf{y} = \mathbf{0},\tag{11.3}$$

where **C** is the stiffness matrix, **M** is the mass matrix, λ is the eigenvalue, **y** is the eigenmode. If these matrices are of a full rank the equation (11.3) has *N* solutions, where N is the number of rows that correspond to nodal d.o.f. The mass matrix of the flexible subsystem may be formed based on shape functions of finite elements or may have a diagonal form as a result of using lumped model. A user determines number and shapes of used eigenmodes. As a rule a set of eigenmodes includes lower eigenmodes.

Calculation of generalized matrices, orthonormalization of modes. Generalized mass and stiffness matrices are calculated using the modal matrix **H**:

$$\overline{\mathbf{M}} = \mathbf{H}^T \mathbf{M} \mathbf{H}, \ \overline{\mathbf{C}} = \mathbf{H}^T \mathbf{C} \mathbf{H}$$

where \overline{M} is the generalized mass matrix, \overline{C} is the generalized stiffness matrix.

The final step of the preparing set of modes is the orthonormalization of columns of the modal matrix based on eigenvalue problem solution with generalized mass and stiffness matrix:

$$(\bar{\mathbf{C}} - \lambda \bar{\mathbf{M}})\bar{\mathbf{y}} = 0 \tag{11.4}$$

Transformed set of modes is formed based on the equation:

$$\overline{\mathbf{H}} = \mathbf{H}\overline{\mathbf{Y}} \tag{11.5}$$

Diagonal form of transformed generalized matrices leads to minimal CPU efforts during the integration of equations of motion. It is the basic advantage of such an approach. Another aim of such transformations is the exclusion of modes that correspond to movement of the flexible subsystem as a rigid body. It is necessary since the movement of the flexible subsystem as a rigid one is defined by *floating frame of reference* CS1. Zero eigenvalues correspond to rigid body modes of flexible subsystem (11.4).

11.1.2. Calculation of stresses and strains

Let us consider the discrete expressions of elasticity theory used in the finite elements method:

$$\boldsymbol{\varepsilon}_{i}^{e} = \mathbf{B}_{i}^{e}(\mathbf{x}_{i}^{e})\mathbf{u}_{i}^{e},$$

$$\boldsymbol{\sigma}_{i}^{e} = \mathbf{D}_{i}^{e}\boldsymbol{\varepsilon}_{i}^{e} = \mathbf{D}_{i}^{e}\mathbf{B}_{i}^{e}\mathbf{u}_{i}^{e},$$
(11.6)

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where $\boldsymbol{u}_{i}^{e}, \varepsilon_{i}^{e}, \boldsymbol{\sigma}_{i}^{e}$ are matrix-columns of nodal degrees of freedom of strains and stresses of *i*-th finite element, \boldsymbol{B}_{i}^{e} is matrix expressing strain field of the finite element with the nodal displacement, \boldsymbol{D}_{i}^{e} is elasticity matrix of the finite element which is generated according to Hooke's law, \boldsymbol{x}_{i}^{e} is matrix-column of coordinates of finite elements nodes. Sizes of the matrices depend on finite element type.

If nodal displacements are represented as the sum (11.2), strains and stresses of a finite element can be represented by following expressions:

$$\boldsymbol{\varepsilon}_{i}^{e} = \mathbf{B}_{i}^{e}(\mathbf{x}_{i}^{e})\mathbf{H}_{i}^{e}\mathbf{w} = \mathbf{B}_{i}^{e}(\mathbf{x}_{i}^{e})\sum_{j=1}^{H}\mathbf{h}_{ji}^{e}w_{j} = \sum_{j=1}^{H}\mathbf{h}_{ji}^{e\varepsilon}w_{j} = \mathbf{H}_{i}^{e\varepsilon}\mathbf{w},$$

$$\sigma_{i}^{e} = \mathbf{D}_{i}^{e}\mathbf{B}_{i}^{e}(\mathbf{x}_{i}^{e})\mathbf{H}_{i}^{e}\mathbf{w} = \mathbf{D}_{i}^{e}\mathbf{B}_{i}^{e}(\mathbf{x}_{i}^{e})\sum_{j=1}^{H}\mathbf{h}_{ji}^{e}w_{j} = \sum_{j=1}^{H}\mathbf{h}_{ji}^{e\sigma}w_{j} = \mathbf{H}_{i}^{e\sigma}\mathbf{w},$$
(11.7)

where \mathbf{h}_{ji}^{e} is the part of j-th mode which corresponds to nodal degrees of freedom of *i-th* finite element. Matrices-columns \mathbf{h}_{ji}^{ez} and $\mathbf{h}_{ji}^{e\sigma}$ represent stresses and strains from nodal displacements of the finite element which are correspond to the mode \mathbf{h}_{ji}^{e} when value of the modal coordinate $w_{i}=1$. These matrices-columns are called *element solutions*.

So far as D_i^e , B_i^e , (x_i^e) are constant matrix, they are not used for simulation after calculation of h_{ji}^{ez} and $h_{ji}^{e\sigma}$. Therefore, stresses and/or strains can be calculated during integration of equations of motion of flexible body if stresses and/or strains modal matrices are calculated correspond to the expressions (11.7). Matrices-columns h_{ji}^{ez} and $h_{ji}^{e\sigma}$ corresponded to the mode h_j of a flexible body are calculated by FEA software. Before using in UM software, they are transformed similarly to the matrices-columns h_j based on the expressions (11.4), (11.5).



Figure 11.2. To example of calculation of nodal stresses

Nodal stresses or strains are calculated by FEA programs based on values which are calculated for elements including the concerned node. The simple averaging of values is often used. For example, if the node with index *i* is belonged to the four finite elements with the indices *j*, *k*, *l*, *m* (Figure 11.2), then nodal stress are calculated as

$$\sigma_i^n = \frac{\left(\sigma_{ji}^e + \sigma_{ki}^e + \sigma_{li}^e + \sigma_{mi}^e\right)}{4} = \frac{\sum_{b \in M_i} \sigma_{bi}^e}{N_i},$$

where σ_i^n is nodal stress, σ_{ji}^e is the stress components in the node *i* of the finite element with the index *j*, M_i is the set of indices of the finite elements including the node *i*, N_i is the count of finite elements including the node *i*.

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UM imports solutions for elements. The nodal solutions are calculated as average values in the elements containing the node.

11.2. Installation, preparing data, workflow

UM FEM installation package includes the following items:

- software for data import from **ANSYS**:
 - macro file **um.mac** for ANSYS, which is written in APDL (*ANSYS Parametric Design Language*);
 - stand alone program for data transformation **ansys_um.exe**;
- software for data import from MSC.NASTRAN:
 - file **umfum.alt** with procedures which are written in DMAP language (*Direct Matrix Abstraction Program*);
 - stand alone program for data transformation **nastran_um.exe**;
- software for data import from **ABAQUS abaqus_um.exe**;
- wizard of flexible subsystems built in UM Input program;
- software procedures for handling and simulation of dynamics of flexible bodies that are built in **UM Input** and **UM Simulation** programs.

Simulation of dynamics of flexible bodies supposes the following steps to be done.

- 1. Creating the FEA model of the flexible body to analyze in the external FEA software.
- 2. Choosing the interface nodes, calculation of the *eigenmodes* and *static modes* according to Craig-Bampton method.
- 3. Exporting data from external FEA software and its transformation to UM format.
- 4. Including the flexible subsystem into hybrid model with the help of **UM Input** program.
- 5. Simulation of dynamics of the hybrid model with the help of **UM Simulation** program.

Every step is considered in the next items. Data preparing in **ANSYS** is described in Sect. 11.2.1. "Exporting finite element model from ANSYS" p. 11-9, Sect. 11.2.2. "Exporting finite element model from MSC.NASTRAN", p. 11-26 is devoted to work in **MSC.NASTRAN**, Sect. 11.2.3. "Exporting finite element model from NX NASTRAN", p. 11-38 is devoted to **NX NASTRAN** and Sect. 11.2.4. "Model creation in ABAQUS environment and data exchange", p. 11-49 is devoted to **ABAQUS**.

11.2.1. Exporting finite element model from ANSYS

11.2.1.1. General information

The whole workflow of the preparing input data for models that include flexible bodies is shown in Figure 11.3. Let us consider basic steps of this procedure.

The first step is executed under **ANSYS** environment. According to the instructions to **AN-SYS** software, the work directory and *JobName* are chosen. *JobName* is a name of all the files for certain FEA model.

After creating the FEA model and choosing interface nodes the macros **um.mac** is executed. The macro has commands for calculation of eigenmodes and static modes, as well as calculation and export of mass and stiffness matrices. As a result of **um.mac** execution, several files are cre-

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ated: standard **ANSYS** result file *JobName.rst*, *JobName.full* that contains matrices of a flexible body that corresponded to fixed interface nodes, *JobName.free* that contains matrices of a free body, and *JobName.mlmp* with a diagonal mass matrix of a free body. In dependence of arguments of the um.mac the *JobName.mlmp* file may not be created. For example, if *Beam* is the task name then files *Beam.rst*, *Beam.full* and *Beam.free* will be created in the working directory after calculations.





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After the installation of UM, the **um.mac** file is situated in the **{um_root}\bin** directory. Copy the **um.mac** file to the directory that is selected as a default directory for the macro files in ANSYS. It is usually **.\docu** directory from the ANSYS root directory. Otherwise you should indicate the path to the **um.mac** file using **PSEARCH** command:

/PSEARCH, path_to_um.mac.

The second step of the data preparing is fulfilled in the **ansys_um.exe** program, which is situated in the **{um_root}\bin** directory. **Ansys_um.exe** may produce the final ready-to-use *input.fss* or *input.fum*, which contains intermediate data. The second way with *input.fum* often is more convenient for further analysis.

Ansys_um.exe can be run automatically right from the **um.mac** or manually. To run **ansys_um.exe** automatically you should open the **um.mac** and edit the last line with the /**sys** command. The argument of this command should be the correct path to the **ansys_um.exe** program. For example,

/sys, c:\um\bin\ANSYS_UM.exe

Note.ANSYS ignores the /sys command if it contains spaces. In order to run an-
sys_um.exe from the um.mac you should copy ansys_um.exe and um.rsc from
the {um_root}\bin to the directory without spaces in path.

The **Wizard of flexible subsystems** (**UM Input** program) gives user additional possibilities for preparing data. Using the *input.fum* the **Wizard** let the user visually control the calculated modes, exclude some modes if necessary and fulfill all the transformations for creating the final *input.fss*.

Further work flow is very similar to modeling with usual subsystems. The *input.fss* file is the standard data file for the flexible subsystem just as *input.dat* is a data file for the whole model. A name of directory that contains *input.fss* is considered as a name of the flexible subsystem.

Describing a hybrid model should be done within **UM Input** program. This program generates a data file of the hybrid model *input.dat*, generates equations of motion and compiles them as *UMTask.dll* file, which is used in the **UM Simulation** program for numerical solving these equations.

Preparing data under **ANSYS** environment includes three basic steps. Let us consider them more detailed.

1. Describing the flexible body in terms of ANSYS according ANSYS User's Guide.

| Note. | It is necessary to use System International for all units. Use the command |
|-------|--|
| | /UNITS,SI |
| Note. | During the preparing the data and creating a FE-mesh it is necessary to provide |
| | creating the nodes of FE-mesh in joint points and points of attaching force ele- |
| | ments. To create nodes of FE-mesh with specified coordinates in body-fixes ref- |
| | erence frame you can set key points there (K command), hardpoints (HPTCRE- |
| | ATE command) or with the help of choosing appropriate parameters of automatic |
| | generation of FE-mesh. |
| | |

- 2. Selection of the *interface nodes* of the FE-mesh of the flexible body with the help of sequence of NSEL commands or combination of the KSEL and NSLK commands. For example, you can select *interface nodes* as following:
 - NSEL,s,,,1,10,1 !selection of a new set of nodes !from #1 to #10, step 1 selection of a new set of nodes that NSEL,s,,,1 !includes one node #1 NSEL,a,,,385 !add one more node #385 to the set of !selected nodes !creating the a set of key points consisted KSEL,s,,,1 !of one key point #1 !add the #23 key point to the set of KSEL,a,,,23 !selected key points !selection of a new set of nodes associated NSLK,S !with selected key points
- 3. Running the **um.mac** macro-command from the **ANSYS** command line: *UM,NEForms,WayM,StressInclude,StrainInclude*

| | NEForms | is required number of eigenmodes correspond to the lowest eigen- |
|-------|---------------|--|
| | | values of the flexible body; |
| | WayM | is a way of forming mass matrix: |
| | | 0 means mass matrix, based on shape functions of finite ele- |
| | | ments; |
| | | 1 means diagonal mass matrix. |
| | StressInclude | calculate stresses corresponding to modes of flexible subsystem |
| | | 1 means 'yes' |
| | | 0 means 'no' |
| | StrainInclude | calculate strains corresponding to modes of flexible subsystem |
| | | 1 means 'yes' |
| | | 0 means 'no' |
| | | |
| Note. | If you su | ppose to run series of calculations with various numbers of eigenmodes |
| | it is reco | mmended that you set maximal number of eigenmodes in NEForms. |
| | Once exp | porting here all the eigenmodes that could be used for all of the calcula- |

tions you will be able to remove some of them later using the Wizard of flexible subsystems.
 Note. The message *«6 RIGID modes defined but only 5 total modes requested. Solution not interesting»* might appear during running UM macros. It is not a critical error and is connected with calculation of mass matrix of a free body. Close the error

message and go on working.

11.2.1.2. Creating stress and strain sensors

The actions needed for creating sensors of stress and strains are similar. Therefore only stress sensors making is described in this item.

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According to FE approach stresses are calculated in the nodes of finite elements. Nodal stress is average value calculating from all finite elements including given node. Just nodal stresses are usually interesting for constructions analysis. In order to calculate nodal stress in **UM**, data file input.fum should contain matrices-columns $h_{ji}^{e\sigma}$ at least for one finite element including this node (see Sect. 11.1.2. "Calculation of stresses and strains", p. 11-6). The nodes are called *sensors* if data for stresses calculation in these nodes is present.

Preparing of data which are needed for stresses calculation in **UM** can require a lot of CPU resources. For some models with greater number of nodes and finite elements, this calculation can be impossible if user tries to prepare data for all of nodes. Size of file which available for reading in **ANSYS_UM** and **UM Input** programs is limited by value of 2 Gb. At the same time, a researcher can interest in stresses only in some nodes which number is not great.

Let us consider two ways which allow calculating data only for selected nodes and thereby reduce computer resources requirement.

11.2.1.2.1. Choice of sensors in ANSYS

First way allows specifying a set of nodes for which stresses will be calculated and saved to result file JobName.rst by **ANSYS**. Before **um.mac** launch, the component ESTRS should be created using CM command.

Example. Create component for stresses or strains calculation in the nodes 17, 24, 138, 1235. The following sequence of APDL command is used.

| NSEL,s,,,17 | !create a new set of nodes which consists | |
|---------------|---|--|
| | !of one node with the number 17 | |
| NSEL,a,,,24 | !add node 24 to the set | |
| NSEL,a,,,138 | !add node 138 to the set | |
| NSEL,a,,,1235 | !add node 1235 to the set | |
| ESLN,s,0,all | !select finite elements which include | |
| | !selected nodes | |
| CM,ESTRS,ELEM | !create component called ESTRS which | |
| | !consists of selected finite elements | |
| ESEL,all | !select all finite elements | |

After execution **um.mac**, the result file will be contained data for stresses calculation in the nodes of elements belonging to ESTRS component only. Thus, size of file JobName.rst can be reduced and computation time can be shortened as compared with the full model. However note that the calculation in **ANSYS** is carried out once at the stage of data preparing and size of file JobName.rst is critical only if it exceed 2 Gb or under the deficit of disc space. Otherwise the second way can be used (see the next item).

Note. Under the execution of **um.mac**, the component ESTRS including a set of selected finite elements is created. Data for the rest elements is not computed and not included in the file input.fum. The last line in the example selects all elements. If model of flexible body consisted of not all elements which are made in **ANSYS**, this line should be edited. But making ESTRS component should be always precede selection of a set of finite element which are included in the file input.fum.

11.2.1.2.2. Choice of sensors in ANSYS_UM

The user can create the list of nodes-sensors. Data for them is selected by **ANSYS_UM** from file JobName.rst and included in the file input.fum (input.fss). The list of the sensors is described in the text file umsensors.lst which should be in the working directory of the task. The file has the following structure. The first line contains the comment starting with symbol «\$»:

\$ UM SENSORS NODES LIST

The second and following lines include numbers of the sensors. One number is per one line. The file can include comments which starting with symbol «\$». It must be in separate lines. For example,

\$ Second section 365

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The Second line must contain one word «ALL» if all nodes must be selected.

UM includes the macro umsensors.mac which helps to create file *umsensors.lst*. Copy umsensors.mac to the **ANSYS** directory which contains macro files by default (for example, .\apdl for version 9 - 11). The command line is as follows:

umsensors,newfile,startnum,finishnum,stepnum

| Newfile | 0 means 'create new list of nodes'; |
|-----------|---|
| | 1 means 'add to existing list'. |
| startnum | is a starting number of node set., |
| | -1 includes all nodes of a finite element mesh to the set, other parameters are |
| | ignored, the list created earlier is deleted. |
| finishnum | is the finish number of the node set. |
| Stepnum | is a step of node number increment, 1 by default; |
| | The one number startnum is added to the set if parameters finishnum and |
| | stepnum are absent. |
| | |

All nodes in which stresses (strains) can be calculated are selected if file *umsensors.lst* is absent in the task directory. If there is no data in the file JobName.rst for stresses calculation in elements which contain node N, inclusion of this number in *umsensors.lst* does not have effect. That is, file input.fum contains data for stresses calculation in the nodes which belong to intersection of sets ESTRS and *umsensors.lst*. The content of input.fum depending on prior actions when parameter *StressInclude* of **um.mac** is equal to 1 is presented in the Table 11.1.

| Tabl | e | 1 | 1 | .1 | |
|------|---|---|---|----|--|
| | | | | | |

| № | Component ES- | JobName.rst | umsensors.lst | input.fum |
|----|----------------|-------------|-----------------------|------------------------|
| | TRS is created | | | (input.fss) |
| 1. | no | all nodes | file is absent or all | all nodes |
| | 110 | annoues | nodes are selected | all nodes |
| 2. | no | all nodes | Umsensors | umsensors |
| 3. | VAC | ESTRS | file is absent or all | FSTPS |
| | yes | | nodes are selected | |
| 4. | yes | ESTRS | Umsensors | ESTRS \cap umsensors |

Simulation efficiency in **UM** directly depends on size of file input.fss. That is appreciably at multivariant calculations (see Sect. 6.2. «Scanning»). Therefore, it is recommended to prepare previously the file *umsensors.lst* if calculating of stresses in the every node of a model is not needed.

11.2.1.3. ANSYS-UM data exchange

The ANSYS_UM.EXE is considered in this section and used for importing data from AN-SYS to UM. It converts data that made by **um.mac** macro and saves this data in UM format.

Input.fss file includes a set of transformed modes without rigid body modes of the flexible subsystem. **UM Input** program directly loads and supports this file for describing flexible subsystems.

Input.fum includes intermediate data that could be transformed with the help of **Wizard of flexible subsystem**. This file contains static modes, eigenmodes and the generalized mass matrix.

Files *.*fum* and *.*fss* are of the same structure and contain information about modes and matrices as well as information about FE-mesh, nodes and elements.

Ansys_um includes the General and Options tabs, see Figure 11.4.

| An Creating data set for simulation of flexible body | 23 |
|--|----|
| File Options Sensors | |
| ANSYS results file (*.rst): | |
| D:\Simulation\ANSYS_TASK\BMZ\RMSimple778.rst | |
| Save to the same directory Target directory: | |
| D:\Simulation\ANSYS_TASK\BMZ\RMSimple778 | õ |
| Create Close | |

Figure 11.4.

The **General** tab (Figure 11.4) lets the user select a*.*rst* file and sets the target directory for saving *input.fum / input.fss* files. It is recommended to create this target directory in advance.

| Creating data set for simulation of flexible body | X |
|---|---|
| File Options Sensors | |
| Transformations | |
| Vormalize modes | |
| Exclude rigid body modes | |
| Frequency: 0.500 | |
| | |
| | |
| | |
| | |
| Create Close | |

Figure 11.5.

The **Options** tab (Figure 11.5) defines structure of output files. The following variants are possible.

- Set of static modes and eigenmodes of the flexible subsystem, the generalized mass and the stiffness matrix (transformations 11.4, 11.5 are omitted). To prepare such a set of data turn off the **normalize modes** flag; the rest control elements are not enabled.
- Set of transformed modes that includes modes of motion as rigid body. To prepare such a set of data turn on the **normalize modes** flag and turn off the **exclude rigid body modes** flag. In this case to finish preparing data it is necessary to exclude rigid body modes later in **Wizard of flexible subsystems**.
- Set of transformed modes, without rigid body modes. Turn on **normalize modes** and **exclude rigid body modes** flags. In this case a value in the **frequency** box defines maximum module of natural frequency that correspond to rigid body motion. This variant of setting leads to creating the files which can be directly loaded in **UM Input** and **UM Simulation** programs.

Notes.

- 1. Severe solution provides zero eigenvalues for eigenmodes that correspond to free body motion. However round-off errors during numerical solution lead to appearing the small nonzero eigenvalues in the spectrum of a problem. Here the **frequency** option is used.
- 2. When coupled mass matrix is used the latter variant is obligatory.
- 3. If you use a diagonal mass matrix it is recommended to use the variant with turned off **nor-malize modes** and then use the **Wizard of flexible subsystems**.

The **Sensors** tab includes control items for writing of data for calculation of stresses and strains. View of right part of the tab is defined by the way of choose of sensors. The left part are invariable.

If the directory of a task includes file umsensors.lst (see 11.3.2.2. "Solution tab", p. 11-79), the tab looks like in Figure 11.6.

The check boxes of the **Include solutions for elements** group allow to include/exclude data for stresses and strains calculation to file input.fum. If the **delete list after transformation** check box is turned on then file *umsensors.lst* is deleted after creating *input.fum*. In most cases, it is recommended turn off this checkbox. Thus sensors list can be used many times.

Set of sensors can be edited via flags in the left part of each element of the list. The popup menu can be used for that (Figure 11.7).

| Creating data set for simulation of flexible body | | |
|---|---|--|
| File Options Sensors | | |
| List of sensors is defined by ○ ANSYS | List of nodes of sensors: total 2709, selected 2703 Node 1 Node 2 Node 3 Node 4 Node 5 Node 6 Node 7 Node 8 Node 8 Node 9 Node 10 Node 11 | |
| Create | | |

Figure 11.6. View of the Sensors tab under choose of nodes-sensors from file umsensors.lst.

| Select all Unselect all |
|----------------------------|
| Sort |
| Refresh |
| |

Figure 11.7.

File *umsensors.lst* can be created, deleted or edited after run of **ansys_um**. Information on the form is refreshed by button is refreshed by button or by item **Refresh** of the popup menu.

If file *umsensors.lst* is absent in the task directory or read error occurred, the message presented in Figure 11.8 appears on the screen and no sensors are output to *input.fum*. The view of form after choosing of sensors in **ANSYS** is presented on Figure 11.9.



Figure 11.8.

| Creating data set for simulation of flexi File Options Sensors | ible body |
|---|---|
| List of sensors is defined by ANSYS umsensors.lst | List of sensors defined in ANSYS program |
| Include solutions for elements: Stresses Strains | |
| Delete list after transformation | |
| Create Close | |

Figure 11.9. Sensors tab

Load a *.*rst* file, select the suitable options and click **Create** button. Preparing output data takes some time that depends on number of nodes, static modes and eigenmodes. Correspondent message informs you about results of calculation.

11.2.1.4. Features of data import from ANSYS Workbench

ANSYS Workbench is a universal finite-element package, suitable for various classes of tasks (strength, thermal physics, fluid and gases dynamics, electromagnetism). This chapter explains how to prepare data of the mechanical FE models for dynamic studies in the UM software.

Let us note the most important points which are significant when importing flexible model from **ANSYS Workbench** software to UM software. To prepare the data the macro **um.mac**, which must be located in the directory **.\apdl** of the **ANSYS Workbench** environment, is used.

Note. SI system must be used, see Figure 11.10.

To import data in the UM software do the following steps.

The first step. Modal analysis should be set. To do this, choose **Modal** in the **Toolbox** taskbar by double-clicking the left mouse button. As a result the outline of a project of modal analysis will appear, see Figure 11.11.

| Units | Extensions Help | | | | |
|---|--|--|--|--|--|
| 🖌 s | iI (kg,m,s,K,A,N,V) | | | | |
| Metric (kg,m,s,°C,A,N,V) | | | | | |
| N | Metric (tonne,mm,s,°C,mA,N,mV) U.S.Customary (lbm,in,s,°F,A,lbf,V) U.S.Engineering (lb,in,s,R,A,lbf,V) | | | | |
| U | | | | | |
| U | | | | | |
| C C | Display Values as Defined | | | | |
| 0 | Display Values in Project Units | | | | |
| Unit Systems | | | | | |

Figure 11.10. SI system



Figure 11.11. Project outline for modal analysis

In the **Design Modeler** module a geometrical rigid model of an object is built. Double-click the left mouse button on the **Geometry** field of the task project to call the module.

The second step. Creating a FE mesh in the **Mechanical** module, which can be activated by double-clicking on the left mouse button on the **Model** field, see Figure 11.12.

The third step. Adding commands in **APDL** language. According to the basic method of the flexible bodies dynamics modeling, a FE model should be described as a superelement, stress and strain sensors have to be chosen. The user is offered to perform all this actions in the **Workbench** environment with the help of the **APDL** commands.

Creation of rigid regions and description of a superelement, creation of stress and strain sensors, as well as the call of the **UM.MAC** macro are made in the **Commands** field in the element tree. The **Commands** field is added with the right mouse button **Modal** -> **Insert** -> **Commands**. In the **COMMANDS** field commands in the **APDL** language are set.

APDL language commands, used to prepare the import in UM are described in detail in Sect. 11.2.1.1. "General information", p. 11-9 and Sect. 11.2.1.2.1. "Choice of sensors in ANSYS", p. 11-14.

In Figure 11.13 you can see a window with commands described above without rigid regions for the platform.

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| 🕑 E | 3 : Modal - Mechanical [ANSYS Multiphysics] – 🕻 | × |
|---|---|---------------------|
|] File Edit View Units Tools Help 🛛 🥥 ↔ 🗍 🏂 Solve 🔻 ?√ Show Errors 🏥 👪 🔯 | 🚸 \Lambda 👰 🔻 🗊 Worksheet 🛛 i | |
|] 🖫 🕂 🐨 b- 1,- b b b b b 🕒 🚳- 5 🕂 C 🕀 🔍 🔍 🔍 🔍 | 🗱 🕼 📾 🗞 🗖 🗸 | |
| 🚽 😤 Selection 🔻 💡 Visibility 🔻 🕞 Suppression 🔻 | | |
| 🛛 🗩 Show Vertices 🦓 Wireframe 🛛 📲 Show Mesh 🥠 🕌 Random Colors 🔗 Annotation Pre | ferences $\downarrow \downarrow \downarrow \downarrow \downarrow$ | |
| ∫ 🚰 ⊖⊷ Reset Explode Factor:) Assembly Center 👻 🛛 🚻 Edg | e Coloring ▼ 0 ▼ 1 ▼ 1⁄2 ▼ 1⁄3 ▼ 1⁄x ▼ 💉 🙌 🗠 Thicken Annotations | |
| Mesh 🗧 Update 🎕 Mesh ▼ 🍕 Mesh Control ▼ 🎕 Mesh Edit ▼ 📲 Metric Graph 🐵 Pi | robe 🛛 💷 🖉 🕶 🕶 | |
| Outline 7 | | |
| Filter: Name ▼ ② ◇>> ① Improject Improject Improject Improj | ANS ANS | 5YS 816.1 |
| Details of "Mesh" * | | |
| Display ^ | | |
| Display Style Body Color Defaults | 0.000 0.200 0.400 (m) | ×γ |
| Selection Information # × | 0.100 0.300 | |
| Coordinate System: Global Coordinate System 👻 🔗 Show Individual and Summary 💌 | Geometry / Print Preview / Report Preview / | |
| No Selection | Messages | φ× |
| | Text Association | |
| | Warming The program has detected an unknown error during the solution or a result file older th Project>Model>Model>Solution C Messages Graphics Annotations | > |
| | Metric (m, kg, N, s, V, A) Radians rad/s Celsius | |

Figure 11.12. An example of a finite-element model of a platform in the Mechanical module

| Commands | | | |
|--|--|--|--|
| ! Commands inserted into this file will be executed just prior to the ANSYS SOLVE command. ! These commands may supersede command settings set by Workbench. | | | |
| ! Active UNIT system in Workbench when this object was created: Metric (m, kg, N, s, V, A) ! NOTE: Any data that requires units (such as mass) is assumed to be in the consistent solver unit system. ! See Solving Units in the help system for more information. | | | |
| NSEL,s,,ALL ESLN,s,O,ALL CM,ESTRS,ELEM ESEL,ALL NSEL,A,L1 NSEL,a,,,1 NSEL,a,,,2 NSEL,a,,,27 UM,15,1,1,1 | | | |
| Graphics Commands | | | |

Figure 11.13. The Commands window with commands in APDL

In this example a set of strain and stress sensors which includes all nodes and elements of the FE model is prepared. Then the interface nodes with the numbers 1, 2, 24 and 27 are chosen and UM macro to calculate the first 15 eigenmodes, stresses and strains is run.

In some cases, for correct simulation results it is required to create **rigid regions** around the interface nodes.

The creation of rigid regions is done either interactively or with the help of the following **APDL** commands:

CERIG, MASTE, SLAVE, Ldof, Ldof2 ... Ldof5, where CERIG is the command to create a rigid connection. MASTE is the main node number, SLAVE is the dependent node number,

Ldof, Ldof2 ... Ldof5 are the degrees of freedom, for which restrictions are imposed.

Note. Degrees of freedom with rigid regions must be valid for the used types of finite elements.

An interactive way to create a rigid region is connected with the creation of the **Point Mass** (mass point) and **Remote Points** elements. To create a **Point Mass** element in the element tree field choose **Geometry** –> **Insert** –> **Point Mass**. In the appeared window set in the **Geometry** field the position in which the mass point will be created, and in the **Mass** field, set up the **Point Mass** value (Figure 11.14).

| Scope | |
|--------------------------|--------------------------|
| Scoping Method | Geometry Selection |
| Applied By | Remote Attachment |
| Geometry | No Selection |
| Coordinate System | Global Coordinate System |
| X Coordinate | 0. m |
| Y Coordinate | 0. m |
| Z Coordinate | 0. m |
| Location | Click to Change |
| Definition | |
| Mass | 0. kg |
| Mass Moment of Inertia X | 0. kg·m² |
| Mass Moment of Inertia Y | 0. kg·m² |
| Mass Moment of Inertia Z | 0. kg·m² |
| Suppressed | No |
| Behavior | Deformable |
| Pinball Region | All |

Figure 11.14. Fields necessary to describe the Point Mass element

Right-click to choose the formed object **Point Mass->Promote to Remote Point**, see Figure 11.15.

In the appeared settings window of a created object **Point Mass – Remote Point** (Figure 11.16), in the **Geometry** field select the nodes that are included in the rigid region, in the **Location** field indicate the node with the main degrees of freedom (an interface node). In the **Behavior** field select **Rigid**, in the **DOF Selection** field set **Manual**. Set **Active** values to the fields of limited degrees of freedom (**X Component**, **Y Component**, **Z Component**, **Rotation X**, **Rotation Z**).

The fourth step. Right-click on the **Modal** -> **Solve** field of the element tree for the implementation of the solution, Figure 11.17. The results of the solution are in the folder of a working project **PROJECT_NAME\dp0\SYS\MECH**.

The fifth step. **Ansys_um.exe** program is run. How to work in it you can find in Sect. 11.2.1.3. "*ANSYS-UM data exchange*", p. 11-16.

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| Insert • |
|--------------------------------|
| Suppress |
| Promote to Remote Point |
| ■ Duplicate ■ Copy メ Cut |
| X Delete ¤ฏิ⊳ Rename (F2) |
| 🗋 Group |

Figure 11.15.

| Scope | | |
|-------------------|--------------------------|--|
| Scoping Method | Geometry Selection | |
| Geometry | No Selection | |
| Coordinate System | Global Coordinate System | |
| X Coordinate | 0. m | |
| Y Coordinate | 10. m | |
| Z Coordinate | 1.e-002 m | |
| Location | Click to Change | |
| Definition | | |
| Suppressed | No | |
| Behavior | Rigid | |
| Pinball Region | All | |
| DOF Selection | Manual | |
| X Component | Active | |
| Y Component | Active | |
| Z Component | Active | |
| Rotation X | Active | |
| Rotation Y | Active | |
| Rotation Z | Active | |

Figure 11.16. Fields necessary to describe an object Point Mass – Remote Point

| itter: Name | | - | | |
|---|---|-------|-------------------------------------|-----|
| Project Image: Comment of the system Image: Comment of t | ilter: Name 🔻 | | 😰 🖉 🗠 | ± 🥘 |
| | Project Model (A4) Model (A4) Coordinate S Model (A4) Model (| yster | 715 | |
| Commerging Clear Generated Data Clear Generated Da | Pre-Str Analysi | ş | Insert Solve | |
| tails of "Modal (A5) oroup All similar Chindren Definition Definition Structural Analysis Type Modal Solver Target Mechanical APDL Options Environment Temperature 22. "C | Comma Soluti | alb | Clear Generated Data Rename (F2) | |
| Definition Open Solver Files Directory Physics Type Structural Analysis Type Modal Solver Target Mechanical APDL Options Environment Temperature 22. °C | tails of "Modal (A5) | | Group Air Similar Children | |
| Physics Type Structural Analysis Type Modal Solver Target Mechanical APDL Options | Definition | | Open Solver Files Directory | |
| Analysis Type Modal Solver Target Mechanical APDL Options Environment Temperature 22. "C | Physics Type | _ | Structural | |
| Solver Target Mechanical APDL Options Environment Temperature 22, *C | Analysis Type | | Modal | |
| Options Environment Temperature 22. *C | Solver Target | | Mechanical APDL | |
| Environment Temperature 22. °C | Options | | | |
| | Environment Temperat | ture | 22. *C | |
| Generate input Only No | Generate Input Only | | No | |

Figure 11.17. Starting solution

Consider the case when the interface node is not located in the model area, but at some distance from it. For example, Fig.



Figure 11.18. Constraint equations at the circular hole

In this example, you need create an interface node in the cylindrical hole of the model, place the mass element there, and create a rigid region around the interface node by linking it to the other nodes of the model.

1. Create a node at a point that does not belong to the model area.

Remote Point-> Insert-> Remote Point

In field **Scoping Method** set **Free Standing**. Enter coordinates X, Y μ Z, and set the name of node at point in field **Pilot Node APDL Name** (in our case the name is **MyNode**).

| D | | | |
|------------|----------------------|--------------------------|--|
| Ξ | Scope | | |
| | Scoping Method | Free Standing 💌 | |
| | Coordinate System | Global Coordinate System | |
| | X Coordinate | 0. m | |
| | Y Coordinate | 0. m | |
| | Z Coordinate | 0. m | |
| | Location | Click to Change | |
| Definition | | | |
| | Suppressed | No | |
| | Pilot Node APDL Name | MyNode | |

2. Add a point mass. Geometry -> Insert -> Point Mass.

Set **Scoping Method**–>**Remote Point**. In field **Remote Point** select created **Remote point**. Enter mass and moment of inertia values.

| - | icope | | |
|---|--------------------------|---------------------------|--|
| | Scoping Method | Remote Point | |
| | Applied By | Remote Attachment | |
| | Remote Points | Remote Point | |
| | Coordinate System | Global Coordinate System | |
| | X Coordinate | 0. m | |
| | Y Coordinate | 0. m | |
| | Z Coordinate | 0. m | |
| Ξ | Definition | | |
| | Mass | 1.e-004 kg | |
| | Mass Moment of Inertia X | 1.e-003 kg·m ² | |
| | Mass Moment of Inertia Y | 1.e-003 kg·m ² | |
| | Mass Moment of Inertia Z | 1.e-003 kg·m ² | |
| | Suppressed | No | |
| | | | |

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3. In our case rigid regions are convenient to do by APDL commands in field Commands. Modal->Insert->Commands.

For example,

CERIG, MyNode, SLAVE, Ldof, Ldof2 ... Ldof5, where

CERIG is the command to create a rigid connection.

MyNode is the main node name,

SLAVE is the dependent node number,

Ldof, Ldof2 ... Ldof5 are the degrees of freedom, for which restrictions are imposed.

11.2.2. Exporting finite element model from MSC.NASTRAN

11.2.2.1. General information

Analysis of a finite element model is realized in **MSC.NASTRAN** by the means of procedures which are written on MSC.NASTRAN DMAP (Direct Matrix Abstraction Program) language. DMAP is a high-level language including compiler.

For solution of typical tasks, **MSC.NASTRAN** gives sets of procedures called *solution sequences* in the user guide of **NASTRAN**. For example, linear and nonlinear static analysis, modal analysis are typical tasks of **NASTRAN**. Type of analysis is selected via SOL operator. Predefined number of sequence is parameter of *SOL* operator.

For example,

SOL 101 is linear static analysis,

SOL 103 is modal analysis.

MSC.NASTRAN allows changing this sequences or writing new sequences using DMAP. Predefined operator sequences can be modified via ALTER operator which adds or deletes operators from standard procedures of **NASTRAN**. This opportunity of DMAP was used for development of procedures which import data to **Universal mechanism** software.

A flexible subsystem is created based on the superelement method. After description of a finite element model, a user should select interface nodes and create a superelement. Necessary data is imported during modal analysis of the superelement.

Rules of preparing data **MSC.NASTRAN** as well as sequence of using software for data import to **UM** are considered bellow step by step. The description of development and analysis of a model including a flexible subsystem imported from **MSC.NASTRAN** is contained in the guide *«Getting started: flexible bodies using UM FEM»*.

MSC.NASTRAN does not have visual development environment. As a rule, the program **MSC.PATRAN** is used for description of finite element model which is analyzed by **MSC.NASTRAN**. Therefore, becoming operations in **MSC.PATRAN** will be considered bellow under the description of necessary actions of user. Input file of **MSC.NASTRAN** is created by **MSC.PATRAN** automatically during analysis of a model. Screen copies with control elements of **MSC.PATRAN 2005** are presented bellow in the item Sect. 11.2.2.3. "ANSYS-UM data exchange", p. 11-16. Dialog windows of others version of the program can be different.

11.2.2.2. Software modules and workflow

UM allows following software for data import from MSC.NASTRAN.

 Module umfumYYYY.alt developed on DMAP programming language saves data to intermediate files geoms.op2 and matrix.op4 in DMAP format. YYYY in the module name is the version number of MSC.NASTRAN. For example, umfum2005.alt is intended for data import from MSC.NASTRAN 2005.

File geoms.op2 contains a finite element model (nodes, finite elements), flexible modes and data for stresses and strains calculations. File matrix.op4 includes generalized matrices of the model.

- 2. Program converter **NASTRAN_UM.EXE** loads files *geoms.op2* and *matrix.op4* and generates *input.fum* file in **UM** format.
- 3. The main stages of making a flexible subsystem based on import from MSC.NASTRAN and its analysis in UM are presented on in Figure 11.19
- 4. Files *umfumYYYY.alt* and **NASTRAN_UM.EXE** are placed in the directory .*bin* after installation of **Universal mechanism** software.

Note.UM 9.0 supports importing data from MSC.NASTRAN 2005, MSC.NASTRAN
2007, MSC MD NASTRAN 2010 and MSC.NASTRAN 2012. Importing data
from other versions of MSC.NASTRAN was not tested.



Figure 11.19. Creating of flexible subsystem using MSC.PATRAN/NASTRAN

11.2.2.3. Preparing data in MSC.PATRAN/NASTRAN environment

The main stages of creating a flexible subsystem

- 1. Making a finite element model of a considered object in **MSC.PATRAN**. The model should be described in the international system of units of measurement (SI). Finite element mesh should include nodes in the joint points and points of attachment of force elements to the subsystem in the complex object. Some features of preparing the finite element models are described in Sect. 11.3.1. "*Animation window*", p. 11-76.
- Choice of interface nodes in accordance with joint points and attachment points of force elements in the UM model and creating a superelement. This stage is implemented in PA-TRAN by the means of following actions.
 - a) Push the **Elements** button of the tools panel (Figure 11.20).



Figure 11.20. Tools panel of MSC.PATRAN

- b) Carry out the following actions in the appeared dialog window (Figure 11.21).
 - Select Action: Create.
 - Select **Object: Superelement**.
 - Enter the name of the superelement into the **Superelement Name** field.
 - Push the **Select Boundary Nodes** button.

| Action: | Create |
|---------------|--------------------|
| | Supereienieni |
| Supereleme | nt List |
| ्र | × |
| | |
| Supereleme | nt Name |
| Bridge6 | |
| Supereleme | nt Description |
| | |
| Element Def | |
| Elenienic Der | |
| | ▲ ▼ |
| | |
| | |
| Sel | ect Boundary Nodes |
| | |
| | -Apply- |

Figure 11.21. Creating of superelement in MSC.PATRAN

• Choose interface nodes by mouse in the window representing finite element model or input their numbers directly on the form (Figure 11.22). Push **OK** button.

| Get Default Boundary Nodes |
|--|
| Select Boundary Nodes Node 29147 |
| Add Remove Selected Boundary Nodes |
| Node 29014 29034 29059 29105 |
| OK Clear |

Figure 11.22. Choose of interface nodes MSC.PATRAN

• Push **Apply** button, Figure 11.21.

If errors are absent, the superelement with the name assigned in the **Superelement Name** field will be created.

Further, modal analysis of the superelement is executed. The operators which are included in the input file for data import as well as corresponding actions in **MSC.PATRAN** are described below.

3. Modal analysis of the superelement. Set type of analysis 103 (Normal modes) in the **Executive Control Section** of an input file **MSC.NASTRAN**.

SOL 103

In **MSC.PATRAN**, calculation parameters are defined via sequence of actions which is briefly described below.

Form calculation job.

The following actions are carried out before selection of the solution type.

- Push **Analysis** button of the tool panel.
- Execute the following actions on the appeared form on the right (Figure 11.23).
 - Choose Action: Analyze.
 - Choose **Object: Entire model**.
 - Choose Method: Full Run.
 - Assign name of the job in the field **Job Name**.

| ····································· | | | |
|---|--|--|--|
| Action: Analyze ▼ Object: Entire Model ▼ Method: Full Run ▼ | | | |
| | | | |
| Code: MSC.Nastran | | | |
| Type: Structural | | | |
| | | | |
| Available Jobs | | | |
| NewSensorsTest | | | |
| ▼ ▼ | | | |
| Job Name | | | |
| NewSensorsTest | | | |
| Job Description | | | |
| MSC.Nastran job created on 07-Aug-09 at 15:57:01 | | | |
| | | | |
| Translation Parameters | | | |
| Solution Type | | | |
| Direct Text Input | | | |
| Subcases | | | |
| Subcase Select | | | |
| Apply | | | |

Figure 11.23. Model analysis form in MSC.PATRAN

Type of solution is selected on the form which appears after clicking the **Solution Type...** button, Figure 11.24.

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Figure 11.24. Choice of solution type in MSC.PATRAN

4. Assign of intermediate output files geoms.op2 and matrix.op4 in the «File management» section of an input file *.bdf like it is shown below ASSIGN OUTPUT2='geoms.op2' UNIT=13 FORM=UNFORMATTED ASSIGN OUTPUT4='matrix.op4' UNIT=15 FORM=UNFORMATTED In MSC.PATRAN, these lines should be written into Analysis | Direct Text in-

put... | File management field.

| Available Jobs | Direct Text Input | | I × |
|---|---|--------------------------|-----|
| Bridge6 | File Management Section | | _ |
| T | ASSION OUTPUT2='geoms.op2' UNIT=13 FORM=UNFORMATTED ASSIGN OUTPUT4='matrix.op4' UNIT=15 FORM=UNFORMATTED | - | 1 |
| Job Name | | | |
| Job Description | | | |
| MSC.Nastran job created on 29-Apr-09 at 08:51:13 | | | |
| | | | - |
| Translation Parameters | C Nastran System Cell Section | Virite to Input Deck | |
| Solution Type | File Management Section | FMS Write To Input Deck | |
| | C Executive Control Section | EXEC Write To Input Deck | |
| Direct Text Input | C Case Control Section | CASE Write To Input Deck | |
| Subcases | C Bulk Data Section | BULK Write To Input Deck | |
| Subcase Select | OK | Reset Cancel | |

Figure 11.25. Assign of intermediate output files in MSC.PATRAN

5. Add the following line in the **Executive Control Section** in order to link up *umfumYYYY.alt* module.

include umfum2005.alt

This is example for **MSC.NASTRAN 2005**. For other versions of the program, specify the corresponding file *umfumYYYY.alt*.

In MSC.PATRAN, this line is written into the Analysis | Direct Text input... | Executive Control Section field.

File *umfumYYYY.dat* should be put to the directory which is included to list of directories for search of modules by **MSC.NASTRAN**. For example, the working directory of **MSC.PATRAN 2005** which is defined as parameter of shortcut default is subdirectory Temp of the Windows system directory. File *umfum2005.dat* can be put to this directory or to the directory *bin* of **MSC.NASTRAN**.

6. Assign SI units in the **Bulk Data Section**:

DTI, UNITS, 1, KG, NEWTON, METER, SECOND

In MSC.PATRAN this line is written into the Analysis | Direct Text input... | Bulk Data Section field.

7. Assign a number of eigenmodes of the superelement in the **Bulk Data Section**. The command lines similar to presented below are used.

SPOINT, 300001, THRU, 300030 SEQSET1,10,0, 300001,THRU,300030

Thirty eigenmodes of the superelement are required to be calculated in this example. As a rule, the eigenmodes corresponding to the lowest eigenvalues are calculated. Definition of the calculation parameters is described below in item 9.

The *SPOINT* operator defines scalar parameters called *scalar points* in the **MSC.NASTRAN** user's guide. In this case, the scalar points are defined as modal coordinates of the superelement. They correspond to eigenmodes of the model fixed in interface nodes. Thirty scalar points are defined in the example. These points are numbered from 300001 to 300030. As a rule, numbers of the points are chosen greater than maximal number of nodes of the finite element model. That

is, the numbers can be defined from 500001 to 500030. Coincidence numbers of scalar points and numbers of internal nodes of a superelement are not allowed.

SEQSET1 operator defines generalized coordinates of a superelement. In this example, the following parameters are used: parameter 10 is number of the superelement; parameter 0 defines scalar points as generalized coordinates of the superelement; the numbers 300001,THRU, 300030 are numbers of the scalar points assigned as generalized coordinates.

- 8. Other calculation parameters are defined with the help **Analysis** | **Subcases...** form. Assign the name of a new set of parameters in the **Subcase Name** field.
- 9. Push **Subcase Parameters...** button and enter parameters of modal analysis into the fields of the appeared windows, Figure 11.26.

| Subcase Parameters |
|--|
| Extraction Method: |
| Frequency Range of Interest |
| Upper = 1000 |
| Estimated Number of Roots = 100 |
| Number of Desired Roots = 30 |
| Diagnostic Output Level: |
| Results Normalization Normalization Method:Mass ▼ |
| Normalization Point = |
| Normalization Component: |
| Number of Modes in Error Analysis = |
| Default Load Temperature = |
| OK Cancel |

Figure 11.26. Parameters of modal analysis in MSC.PATRAN software.

In the presented example, it is required to calculate thirty eigenmodes corresponding to lowest eigenvalues in the range from 0 to 1000 Hertz by Lanczos method. The number of eigenmodes should be equal to the number of the scalar points defined in Step 7 by SPOINT operator. Calculated modes are normalized relatively mass matrix (M-norm). This normalization method should always be chosen under preparing data for export to **UM**. 10. Open **Output Requests...** form. One element should be in **Output Requests** list of this form:

VECTOR(SORT1,REAL)=ALL

Add this element from list **Select Result Type** if it was not added by default. Delete all other elements from the list if any.

11. In order to create stress or/and strain sensors, write the set of commands similar to following example into the **Subcase** section.

SET 501 = ALL STRESS(CORNER)=501 SET 502 = 101,111,120 THRU 136, 170 STRAIN(CORNER) = 502 OUTPUT(POST) SET 101 = ALL SURFACE 11 SET 101

Let us briefly consider used commands.

SET defines a set of numbers of finite elements for which stresses or strains are calculated. 501 is the number of set. It can be chosen at will among numbers not defined earlier. Reused number as parameter SET command redefines set of finite element numbers.

STRESS calculates stresses in elements. The number of set is specified after the equality sign. The parameter CORNER in brackets is written if elements CQUAD4 are presented in the set. If this parameter is not specified, stresses are calculated only in the center of the elements CQUAD4.

STRAIN calculates strains in elements.

OUTPUT separates the commands of different types. The parameter POST starts output of stresses and strains.

SURFACE defines a surface for calculation of stresses and strains. The command is used for a set of shell elements. If calculation of stresses in solid elements is needed, the VOLUME command is used. For example,

VOLUME 11 SET 101

In this example, the set 501 includes all finite elements; the set 502 consists of finite elements 101, 111, from 120 to 136 and 170.

In order to create a sensor in a node in **UM** software, all elements which include this node should be specified in the set for STRESS or STRAIN command.

In MSC.PATRAN, the commands for creating of sensors are written in the field Analysis | Subcases | Direct text input.

- 12. Select superelement created in p. 2.2 in the **Available Superelements** list on the form which is called by **Select Superelements...** button (Figure 11.27). Press the **OK** button.
- 13. Press the **Apply** button of the **Subcases** form. In the issue, new set of parameters (subcase) for calculation of the superelement will be created. In the next time it should be selected in the **Subcase Select** form which is called on the **Analysis** form.
- 14. Select the created subcase.
- 15. Calculate the model in **MSC.NASTRAN** by the **Apply** button on the **Analysis** form. If the calculation is successful, files geoms.op2 and matrix.op4 will be created in the working di-

rectory. Diagnostics messages are outputted in the file JobName.f06. This information can be useful if there are calculation errors.

16. The job is saved in the database (db file) and it can be selected next time in the list of **Analysis** form.

| Select Superelements: | | |
|--|--|--|
| Available Superelements | | |
| Bridge Residue SE(0) | | |
| C Select All O Unselect All | | |
| Write PART Superelement | | |
| Calculate Component Modes (AUTOQSET) | | |
| Write Superelement Generation and Assembly (SEALL) | | |
| Uncoupled Solution (FIXEDB) | | |
| Superelement Tree Definition | | |
| OK Defaults Cancel | | |

Figure 11.27. Window of Select Superelements...

11.2.2.4. MSC.NASTRAN to UM data exchange

Run NASTRAN_UM.EXE program for making input.fum file. Select geoms.op2 in the working directory of MSC.NASTRAN and specify target directory for input.fum. The flags **Stresses** and **Strains** enable/disable the output of corresponded data to file input.fum, Figure 11.28. This data, of course, must be calculated by MSC.NASTRAN using commands specified in Sect. 11.2.2.3. "ANSYS-UM data exchange", p. 11-16, Step 11 of the list.
| 🚆 Creating data set for sim | ulation of flexible | body | × | | | | | | | |
|--|------------------------|---------------------|---|--|--|--|--|--|--|--|
| Paths to data | | | | | | | | | | |
| G:\Simulation\NASTRAN_TASKS\Platform\geoms.op2 | | | | | | | | | | |
| Save to the same directory | | | | | | | | | | |
| Target directory: | | | | | | | | | | |
| G:\Simulation\NASTRAN_TASKS\Platform | | | | | | | | | | |
| Data was calculated by program | nm | | | | | | | | | |
| C MSC.NASTRAN 2005 | | MSC MD NASTRAN 2010 | | | | | | | | |
| C MSC.NASTRAN 2007 | | C NX NASTRAN 8.0 | | | | | | | | |
| Description | | | | | | | | | | |
| ● Enter | | C Input from file | | | | | | | | |
| File | | | | | | | | | | |
| G:\Simulation\NASTRAN_TA | SKS\Platform\Platfor | m.bdf | | | | | | | | |
| Information input | | | | | | | | | | |
| Solution name: Platfor | m | | | | | | | | | |
| Comment: Car bo | dy | | | | | | | | | |
| Date and time | Diete (dd:ppp://www.it | 06.11.2013 | | | | | | | | |
| Sustem | Date (dd.mm.yyyy). | 00.11.2013 | | | | | | | | |
| C Enter | Time (hh.mm.ss): | 18:15:17 | | | | | | | | |
| Include solutions for elements: | | | | | | | | | | |
| Stresses | | | | | | | | | | |
| 🗖 Strains | | | | | | | | | | |
| Create Close | | | | | | | | | | |

Figure 11.28. Window of NASTRAN_UM.exe program

Solution name, comment and date of calculation can be inputted into corresponded fields of the form or can be read from files *JobName.bdf* or *JobName.f06*. This data is attributes of an **UM** model which are written to file input.fum.

Perform data transformation by the **Create** button. If it is successful, file input.fum will be created in the target directory. Further work with this file is described below in Sect. 11.2.3. *"Exporting finite element model from MSC.NASTRAN"*, p. 11-26.

11.2.3. Exporting finite element model from NX NASTRAN

11.2.3.1. General information

Export of finite element models from **NX NASTRAN** is implemented using DMAP (Direct Matrix Abstraction Program) language. DMAP is a high-level language including compiler.

For solution of typical tasks **NX NASTRAN** gives sets of procedures called *solution sequences* in the user guide of **NX NASTRAN**. For example, linear and nonlinear static analysis, modal analysis are typical tasks of **NASTRAN**. Type of analysis is selected via SOL operator. Predefined number of sequence is parameter of SOL operator.

For example,

SOL 101 is linear static analysis,

SOL 103 is modal analysis.

NX NASTRAN allows changing this sequences or writing new sequences using DMAP. Predefined operator sequences can be modified via ALTER operator which adds or deletes operators from standard procedures of **NASTRAN**. This opportunity of DMAP was used for development of procedures which import data to **Universal mechanism** software.

A flexible subsystem is created based on the superelement method. After description of a finite element model, a user should select interface nodes and create a superelement. Necessary data is imported during modal analysis of the superelement.

Rules of preparing data **NX NASTRAN** as well as sequence of using software for data import to **UM** are considered bellow step by step. The description of development and analysis of a model including a flexible subsystem imported from **MSC.NASTRAN** is contained in the guide *«Getting started: flexible bodies using UM FEM»*.

NX NASTRAN does not have visual development environment. As a rule, the program **FEMAP** is used for description of finite element models for **NX NASTRAN**. Therefore below **FEMAP** commands and operations will be considered. Input file for **MSC.NASTRAN** is created by **FEMAP** automatically during analysis of a model. Screen copies with control elements of **FEMAP 10.3.0** are presented below. Dialog windows of others version of the program might be different.

11.2.3.2. Software modules and workflow

UM provides the following software for data import from NX NASTRAN.

- 1. Module umfumNX**.alt is developed in DMAP language. It saves data to intermediate files geoms.op2 and matrix.op4 in DMAP format. File geoms.op2 contains a finite element model (nodes, finite elements), flexible modes and data for stresses and strains calculations. File matrix.op4 includes generalized matrices of the model.
- 2. Converter **NASTRAN_UM.EXE** loads files geoms.op2 and matrix.op4 and generates input.fum file in **UM** format.
- 3. The main stages of preparing a flexible subsystem based on import from **MSC.NASTRAN** and its analysis in **UM** are presented on in Figure 11.29.

4. File umfumNX**.alt and **NASTRAN_UM.EXE** are placed in the directory .\bin after installation of **Universal mechanism** software.

Note.UM 9.0 supports importing from NX NASTRAN 8.0 and NX NASTRAN 9.0.Importing data from other versions of NX NASTRAN was not tested.



Figure 11.29. Creating of flexible subsystem using MSC.PATRAN/NASTRAN

11.2.3.3. Preparing data in NX NASTRAN/FEMAP environment

The main stage of creating a flexible subsystem

- 1. Making finite element model of a considered object in **MSC.PATRAN**. The model should be described in the international system of units of measurement (SI). Finite element mesh should include nodes in the joint points and points of attachment of force elements to the subsystem in the complex object. Some feature of preparing the finite element models are described in Sect. 11.3.1. "*Animation window*", p. 11-76.
- 2. Choice of interface nodes in accordance with joint points and attachment points of force elements in the UM model and creating a superelement. This stage is implemented in FE-MAP by the means of *Constraints*. Create new constraint set using Model → Constraint → Create/Manage Set named, for example, *InterfaceNodes*, see Figure 11.30. Then use Model → Constraint → Nodal command to fix all degrees of freedom for interface nodes, see Figure 11.31.

| New Constraint Set | | | | | | | | |
|-------------------------------------|------|------------|--|--|--|--|--|--|
| ID 1 Title InterfaceNodes | | | | | | | | |
| Set Type Standard | More | <u>o</u> k | | | | | | |
| C Nastran SPCADD/MPCADD Combination | | Cancel | | | | | | |

Figure 11.30. Creating new constraint set in FEMAP

| Create Nodal Constraints/DOF | | × | | | | | | | | |
|---------------------------------|-----------------------------|-----|--|--|--|--|--|--|--|--|
| Constraint Set 1 InterfaceNodes | | | | | | | | | | |
| Title | oord Sys 0Basic Rectangular | - | | | | | | | | |
| Color 120 Palette Layer 1 | | | | | | | | | | |
| | X Symmetry X AntiSym | w I | | | | | | | | |
| | Y Symmetry Y AntiSym | | | | | | | | | |
| | Z Symmetry Z AntiSym | | | | | | | | | |

Figure 11.31. Creating nodal constrains in FEMAP

- 3. Create a new analysis set using **Model** \rightarrow **Analysis** command, Figure 11.32.
 - (1) Input the title of the analysis set and select **2..Normal Modes/Eigenvalue** in **Analysis Type** field, Figure 11.33.
 - (2) Assign the intermediate output files *geoms.op2* and *matrix.op4* as it is shown below, Figure 11.34.

ASSIGN OUTPUT2='geoms.op2' UNIT=13 FORM=UNFORMATTED

ASSIGN OUTPUT4='matrix.op4' UNIT=15 FORM=UNFORMATTED

(3) Add the following line to window shown in Figure 11.35 in order to link up um-fumNX**.alt module.

include umfumNX**.alt

File umfumNX**.alt should be placed into the directory where it can be found by **NX NASTRAN**.

| 🔜 Analysis Set Manager (Active: None) | |
|---------------------------------------|--------------------------|
| No. Applyris Sate Dafiood | |
| NO Analysis Sets Denned | Analyze |
| | <u>A</u> nalyze Multiple |
| | Export |
| | Active |
| | Preview Input |
| | MultiSet |
| | <u>С</u> ору |
| | <u>D</u> elete |
| | Load |
| | |
| | <u>5</u> ave, |
| | <u>N</u> ew |
| | <u>E</u> dit |
| | Done |

Figure 11.32. Creating a new analysis set in FEMAP

| Analysis Set | | × |
|--------------------------|--------------------------|---|
| <u>T</u> itle Analyse | | |
| Analysis <u>P</u> rogram | 36NX Nastran | • |
| <u>A</u> nalysis Type | 2Normal Modes/Eigenvalue | - |
| | Run Analysis Using VisQ | |
| Ne <u>x</u> t | <u>O</u> K Cancel | |

Figure 11.33. Assignment of analysis type in FEMAP

| Universal Mechanism 9 | 1 | 1-43 | Part 11. Simul | ation of fle | exible | bodies |
|---|--|-------------------------------|---|--------------------------------------|--------|--------|
| NASTRAN Executive and Solution Options | | × | | | | |
| Direct Output To | | | | | | |
| Executive Control Problem ID Solution Override Max Time (in minutes) Diagnostics System Cells Extended Error Messages Extended Solution Status Monitoring | MSC/MD Nastran Version Ver 2001 Ver 2004 or later Previous Versions Iterative Solver Number of Processors Solver Memory (Mb 0=Auto) 0 | Analysis Text | : >< 8 >< 4 >< 5 >< T2='geoms.op2'UNIT=18 FORM=UN T4='maurix.op4'UNIT=18 FORM=U | 6 >< 7 >< 8 FORMATED NFORMATED | × 9 × | 10 > |
| Restart Control Saye Databases for Restart Erom Manual Control Sign Standard Executive Control Prev Next | Previous Analysis | Text From File C As Text C | As INCLUDE StatementSelect File | Delete Al | QK Ca | » » |

Figure 11.34. Assignment of intermediate output files geoms.op2 and matrix.op4

| NASTRAN Executive and Solution Options | × | | 🔜 Analys | sis Text | | | | | | | | | | | | | | | | _ | |
|--|---|---|----------|---------------------|----------|----------|-------|---|-----------|-----|---|---|-------|---|---|---|----|---|------|----|--------|
| Direct Output To | | H | < 1 | ~ | 2 >< | 3 | >< | 4 | >< | 5 | ~ | 6 | ~ | 7 | ~ | 8 | >< | 9 | ~ | 10 | > |
| Executive Control Problem ID Solution Override Max Time (in minutes) Diagnostics System Cells V Extended Error Messages C Extended Error Messages | MSC/MD Nastran Version © Ver.2001 © Ver.2004 or later © Previous Versions Solution Options Iterative Solver 00ff Number of Processors 0 Solver Menory (Mt D=0.th) 0 | | 18210 | de umi | | | | | | | | | | | | | | | | | |
| Restart Control Saye Databases for Restart From Manual Control Sign Standard Executive Control Prev Negt Scratch Files | Previous Analysis | | Text Fro | om File — Text C | As INCLU | DE State | cmcnt | | Select Fi | ile | | D | elete | | [| | Ōĸ | | Canc | 4 | × × |

Figure 11.35. Linking umfumNX**.alt module

(4) The number of needed eigenmodes should be set in the window that is shown in Figure 11.36. For that use the following commands.

SPOINT, 300001, thru, 300030

QSET1, 0, 300001, thru, 300030

Thirty eigenmodes of the superelement are required to be calculated in this example. As a rule, the eigenmodes corresponding to the lowest eigenvalues are calculated.

The SPOINT operator defines scalar parameters called *scalar points* in the **NX NASTRAN** user's guide. In this case, the scalar points are defined as modal coordinates of the superelement. They correspond to eigenmodes of the model fixed in interface nodes. Thirty scalar points are defined in the example. These points are numbered from 300001 to 300030. As a rule, numbers of the points are chosen greater than maximal number of nodes of the finite element model. That is, the numbers can be defined from 500001 to 500030. Coincidence numbers of scalar points and numbers of internal nodes of a superelement are not allowed.

SEQSET1 operator defines generalized coordinates of a superelement. More detailed information about command mentioned above one can find in the **NX NASTRAN** user's manual. (5) Set parameters in NASTRAN Modal Analysis dialog window, Figure 11.37.

In the presented example, it is required to calculate thirty eigenmodes corresponding to lowest eigenvalues in the range from 0 to 1000 Hertz by Lanczos method. The number of eigenmodes should be equal to the number of the scalar points defined in Step 7 by SPOINT operator. Calculated modes are normalized relatively mass matrix (M-norm). This normalization method should always be chosen under preparing data for export to **UM**.

(6) Open the dialog window that is shown in Figure 11.38 and copy the following command:

VECTOR(SORT1,REAL)=ALL

This command defines the output format of displacement vector.

| NASTRAN Bulk Data | Options | X | | | | | | | | | | | | | |
|-------------------|---------------------------|--------------------------------------|-----|----------------------------|-------------|-----------|---|------------------|-------|-----|------------|---|-------|------|----|
| Portion | of Model to Write 0Entire | Model | | Analysis Text | | | | | | | | | | _ 10 | 71 |
| PARAM | | Format | | | | | | e | _ | | | | | 0 | - |
| AUTOSPC | 0Eigenvalue | Small Field | | SPOINT, 901001, thru. | 901021 | ~ - | ~ | • ~ | · · · | ~ • | ~ | - | ~ | | |
| GRDPNT | 0 | C Large Field (CSys, Material, Prop) | 4 | QSET1, 0, 901001, thr | u, 901021 | | | | | | | | | | |
| WTMASS | 1, | C Large Field (Csys, Node) | 117 | | | | | | | | | | | | |
| □ K6ROT | 100. | C Large Field (All But Elements) | | | | | | | | | | | | | |
| | 10000000 | C Large Held | | | | | | | | | | | | | |
| | 0.01 | Translator Options | | | | | | | | | | | | | |
| | 0,01 | All Plates as QUADR/TRIAR | | | | | | | | | | | | | |
| | -10n 💌 | Skip Beam/Bar Cross Sections | | | | | | | | | | | | | |
| I BOLTFACT | 1000000, | Rigid Element Thermal Expansion | | | | | | | | | | | | | |
| ENFMOTN | 0Constraint Mode 💌 | Gaps as Contact | | | | | | | | | | | | | |
| LANGLE | AUTOMPC | Dynamic Loads using LOADSET/LS | | | | | | | | | | | | | |
| LGDISP | DDRMM off | Write All Static Load/BC Sets | | | | | | | | | | | | | |
| LGSTRN | MODACC | Manual Control | | | | | | | | | | | | | |
| PRGPST | RESVEC | Skip Standard Bulk Data | | | | | | | | | | | | | |
| GEOM | C On C Off | End Text at End of File Outside Bulk | | | | | | | | | | | | | |
| SRCOMPS | RESVINER | | | T | | | | | | | | | | Þ | Ě |
| | | Start Text (On) End Text (Off) | | Text From File | | | | | | | | | | 12 | 1 |
| Prev | Ne <u>x</u> t | OK Cancel | | As Text As INCLUDE Sta | atement Sel | lect File | | <u>D</u> elete / | U | | <u>о</u> к | | Cance | | |

Figure 11.36. Scalar points

| NASTRAN Modal Analysis | | | × |
|------------------------------|-------------------------|-------------------|-----------|
| Skip EIGx | | Method <u>I</u> D | 1 |
| Real Solution Methods | Range of Interest | | |
| Lanczos | | Real | Imaginary |
| C Auto (HOU/MHOU) | | | |
| O Subspace | From (Hz) | 0, | 0, |
| Legacy Real Solution Methods | <u>T</u> o (Hz) | 0, | 0, |
| C Givens | Eigenvalues and Eige | envectors | |
| O Modified Givens | Eigenvalues and Eige | | |
| C Inverse Power | Number Estimated | | 0 |
| C Inverse Power/Sturm | Num <u>b</u> er Desired | | 30 |
| C Householder | | | |
| O Modified Householder | Normalization Metho | d | Mass |
| Complex Solution Methods | C Mass Node ID | 0 | C Default |
| C Hessenberg | C Paint DOE | 0 | C Courped |
| C Complex Inverse Power | C Fourc | | Coupled |
| C Complex Lanczos | Complex Solution Op | tions | |
| | Convergence | | 0, |
| © Direct | Region Width | | 0, |
| C Modal | Overall Damping (G) | | 0, |
| | | | |
| Prev Ne <u>x</u> t | | <u>O</u> K | Cancel |

Figure 11.37. Parameters of modal analysis

(7) In order to create stress or/and strain sensors, place the following list of commands after VECTOR command, see Figure 11.38.

SET 501 = ALL STRESS(CORNER)=501 SET 502 = 101,111,120 THRU 136, 170 STRAIN(CORNER) = 502 OUTPUT(POST) SET 101 = ALL SURFACE 11 SET 101 Let us briefly consider used commands.

SET defines a set of numbers of finite elements for which stresses or strains are calculated. 501 is the number of set. It can be chosen at will among numbers not defined earlier. Reused number as parameter SET command redefines set of finite element numbers.

STRESS calculates stresses in elements. The number of set is specified after equals sign. The parameter CORNER in brackets is written if elements CQUAD4 are presented in the set. If this parameter is not specified, stresses are calculated only in the center of the elements CQUAD4.

STRAIN calculates strains in elements.

OUTPUT separates the commands of different types. The parameter POST starts output of stresses and strains.

SURFACE defines a surface for calculation of stresses and strains. The command is used for set of shell elements. If calculation of stresses in solid elements is needed, the VOLUME command is used. For example,

VOLUME 11 SET 101

In this example, the set 501 includes all finite elements; the set 502 consists of finite elements 101, 111, from 120 to 136 and 170.

In order to create a sensor in a node in **UM** software, all elements which include this node should be specified in the set for STRESS or STRAIN command.

| Master Requests and Conditions Case ID 0 Iitle 0 Manual Control Skip Standard Prev Next Q | Start Tex | xt (Off) tt (On) Cancel | | | | | | | | | | | |
|---|-----------|-------------------------------|---|----------|---------|---|---|---|------------|---|-----|-----|--------------|
| 🔜 Analysis Text | | | | | | | | | | | | | <u>– 🗆 ×</u> |
| < 1 >< 2 >> 3 | ≻< 4 | ≻< 5 | ~ | 6 | ~ | 7 | ~ | 8 | * | 9 | ~ | 10 | > |
| VECTOR (SORT1, REAL) =ALL SET 1001 = ALL STRESS = 1001 SET 1002 = ALL STRAIN = 1002 OUTPUT (POST) SET 101 = ALL VOLUME 11 SET 101 | | | | | | | | | | | | | × |
| Text From File • As Text © As INCLUDE Stater | nent | Select File | | <u> </u> | elete A | I | [| | <u>O</u> K | | Can | cel | |

Figure 11.38. Stress/strain sensors

(8) Click Next to come to Boundary Conditions dialog window. Select 0..None in Constraints list, Figure 11.39. Select the set of interface nodes described above in Master (ASET) field. Click OK to finish preparing Analysis Set. Later use the Model Info panel to select this analysis set.

| Boundary Conditions | | | | | | | | | | | |
|------------------------------|----------------------|--|--|--|--|--|--|--|--|--|--|
| Primary Sets | | | | | | | | | | | |
| <u>C</u> onstraints | 0None | | | | | | | | | | |
| Loads | 0None | | | | | | | | | | |
| Initial Conditions | 0None | | | | | | | | | | |
| Constraint <u>E</u> quations | 0From Constraint Set | | | | | | | | | | |
| Bolt Preloads | 0From Load Set | | | | | | | | | | |
| Other DOF Sets | | | | | | | | | | | |
| M <u>a</u> ster (ASET) | 1InterfaceNodes | | | | | | | | | | |
| Kinematic (<u>S</u> UPORT) | 0None | | | | | | | | | | |
| SUPORT1 | 0None | | | | | | | | | | |
| OMIT | 0None | | | | | | | | | | |
| QSET | 0None | | | | | | | | | | |
| CSET | 0None | | | | | | | | | | |
| <u>B</u> SET | 0None | | | | | | | | | | |
| Prev Ne <u>x</u> t | QK Cancel | | | | | | | | | | |

Figure 11.39. Define boundary conditions

4. Select the just created analysis set.

5. Click **Analyze** to run the analysis set. If the calculation is successful, files geoms.op2 and matrix.op4 will be created in the working directory. Diagnostics messages are outputted in the file JobName.f06. This information can be useful if there are calculation errors.

11.2.3.4. NX NASTRAN to UM data exchange

Run NASTRAN_UM.EXE program for making input.fum file. Select geoms.op2 in the working directory of NX NASTRAN and specify target directory for input.fum. The flags Stresses and Strains enable/disable output of corresponded data to file input.fum, Figure 11.28. This data, of course, must be calculated by MSC.NASTRAN using commands specified in the Sect. 11.2.2.3. "ANSYS-UM data exchange", p. 11-16, Step 3.7 of the list.

| 🚆 Creating data set for si | mulation of flexible | e body | × | | | | | | | |
|---|----------------------|-----------------------|---|--|--|--|--|--|--|--|
| Paths to data Path to file geoms.op2: | | | | | | | | | | |
| D:\Simulation\NX NASTRAN\Motor Axle\geoms.op2 | | | | | | | | | | |
| 🔽 Save to the same directory | | | | | | | | | | |
| Target directory: | Mater Aula | | | | | | | | | |
| | | | | | | | | | | |
| Data was calculated by progra | amm | • | | | | | | | | |
| C MSC.NASTRAN 2005 | | O MSC MD NASTRAN 2010 | | | | | | | | |
| C MSC.NASTRAN 2007 | | NX NASTRAN 8.0 | | | | | | | | |
| Description | | | | | | | | | | |
| © Enter | | O Input from file | | | | | | | | |
| File | | | | | | | | | | |
| | | | | | | | | | | |
| Information input | | | | | | | | | | |
| Solution name: Axle | | | | | | | | | | |
| Comment: Moto | raxle | | | | | | | | | |
| Date and time | Date (dd:mm:uuuu): | 06 11 2013 | | | | | | | | |
| System | T: (1) | 40.00.51 | | | | | | | | |
| C Enter | l ime (hh.mm.ss): | 18:23:51 | | | | | | | | |
| Include solutions for elements | | | | | | | | | | |
| ✓ Stresses | | | | | | | | | | |
| 🗖 Strains | | | | | | | | | | |
| Create Close | | | | | | | | | | |

Figure 11.40. NASTRAN_UM.exe main window

Solution name, comment and date of calculation can be inputted into corresponded fields of the form or can be read from files JobName.bdf or JobName.f06. This data is attributes of an **UM** model which are written to file input.fum.

Perform data transformation by the **Create** button. If it is successful, file input.fum will be created in the target directory. Further work with this file is described below in Sect. 11.2.5. "*Exporting finite element model from NX NASTRAN*", p. 11-38.

11.2.4. Model creation in ABAQUS environment and data exchange

11.2.4.1. General information

Figure 11.41 represents a complete cycle of preparation of source data using the ABAQUS program and analysis of the model in UM.

Elastic subsystem is created on the basis of the superelement method. After development of the finite element model, user should choose the interface nodes and create the superelement. The necessary data is imported during the modal analysis of the superelement.

Now we will describe the rules for preparing source data in ABAQUS and also the structure and sequence of the software use to import data in **Universal mechanism**.

Step-by-step description of the development and model analysis, which includes imported elastic subsystem, is listed in the manual "Getting started to work in "Universal mechanism software package": a module for simulation of elastic bodies".

11.2.4.2. Software structure, import scheme

For importing from **ABAQUS software package UM** provides the **ABAQUS_UM.EXE** conversion program that reads the file *.fil and generates an input.fum file, that is, saves the data in the **UM** format.

The **ABAQUS_UM.EXE** conversion program after installing the universal mechanism program is located in the directory .\bin. Now we will describe in detail the preparation of the data.

Note. UM 9.0 supports data import only from ABAQUS 6.12-1. The import data on deformations and stresses from the ABAQUS 6.12-1 program is not supported.



Figure 11.41. Creating a flexible subsystem using ABAQUS

11.2.4.3. Preparing data in ABAQUS environment

The basic steps of creating elastic subsystem

- 1. The creation of the finite element model of the analyzed object in the **ABAQUS** program. The model is described in the SI-system of units. The finite element mesh must contain nodes in the hinge points and points of attachment of the strength elements. Some features of creation of the finite element model are described in Sect. 11.2.5. *"Some* features related to preparing FE models", p. 11-66.
- 2. To create a step of calculating the natural frequencies in the **ABAQUS** program go to the **STEP** module (Figure 11.42).



Figure 11.42. How to go to the **STEP** module in the **ABAQUS** program

Using the **Create Step** button ((or double-click on the element (Steps (1) of the model tree or by using **Step** \rightarrow **Create** menu command), create a new calculation step. As a result, **Create Step** window should appear (Figure 11.43), where the initial calculation step is defined. In this window set the name of the step of calculation as Frequency, in the **Procedure type** drop-down list select **Linear perturbation** and choose **Frequency** as a calculation step.

Click the **Continue** button to go to the parameters window of the **Edit Step** calculation step, (Figure 11.44). In the **Edit Step** window on the **Basic** tab in the **Description** column set the name of the current task as Frequency and specify the number of natural frequencies. On the **Other** tab of the **Edit Step** (Figure 11.45) select the value of parameter **Normalize eigenvectors** by equal to **Mass**. Complete the assignment of parameters of the calculation of natural frequencies by pressing the **OK** button.

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| Create Step | | | |
|---------------------------------------|--|--|--|
| Name: Frequency | | | |
| Insert new step after | | | |
| Initial | | | |
| | | | |
| | | | |
| | | | |
| | | | |
| Procedure type: Linear perturbation 💌 | | | |
| Buckle | | | |
| Frequency | | | |
| Static, Linear perturbation | | | |
| Steady-state dynamics, Direct | | | |
| Substructure generation | | | |
| | | | |
| | | | |
| | | | |
| Continue Cancel | | | |

Figure 11.43. Creating **Frequency** calculation step

| 🔶 Edit Step |
|---|
| Name: Frequency |
| Type: Frequency |
| Basic Other |
| Description Frequency |
| Nlgeom: Off |
| Eigensolver: Lanczos Subspace AMS |
| Number of eigenvalues requested: O All in frequency range |
| ⊙ Value: 10 |
| Frequency shift (cycles/time)**2: |
| Minimum frequency of interest (cycles/time): |
| Maximum frequency of interest (cycles/time): |
| ✓ Include acoustic-structural coupling where applicable |
| Block size: O Default O Value: |
| Maximum number of block Lanczos steps: Default C |
| Use SIM-based linear dynamics procedures |
| |
| Include residual modes |
| |
| |
| OK Cancel |

Figure 11.44. Setting of parameters for calculating natural frequencies

| 🖶 Edit Step | × |
|---|---|
| Name: Frequency | |
| Type: Frequency | |
| Basic Other | |
| Equation Solver | |
| Matrix storage: C Use solver default C Unsymmetric C Symmetric | |
| Warning: The analysis code may override your matrix storage choice. See *STEP, UNSYMM in the Abagus Keywords Reference Manual. | |
| Normalize eigenvectors by: C Displacement C Mass | |
| Evaluate dependent properties at frequency: | |
| | |
| | |
| | |
| | |
| | |
| | |
| | |
| | |
| | |
| | |
| | |
| OK Cancel | |

Figure 11.45. Setting of parameters for calculating natural frequencies (continuation)

Then in the interface nodes set the boundary conditions for the step of calculating Frequency. To do this click twice on the item **BCs** in the model tree in the section of the created Frequency calculation step (Figure 11.46).

In the appeared window **Create Boundary Condition** choose the category of boundary conditions **Mechanical** boundary conditions **Displacement/Rotation** and push **Continue** button (Figure 11.47). Then you need to either choose the interface nodes using mouse in the graphic window, or use a pre-generated set of nodes **Set**. Then click the **Done** button at the bottom of the graphic window (Figure 11.48).

In the appeared **Edit Boundary Condition** window choose the fixed degrees of freedom (Figure 11.49).

Note. Fixed degrees of freedom in the **Edit Boundary Condition** window should be acceptable for the types of finite-elements used in model.



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Figure 11.46. How to create boundary conditions for Frequency calculation step

| - Create Boundary C | ondition 🔀 |
|---|--|
| Name: BC-1 Step: Frequency | _ |
| Category Category Mechanical C Fluid C Electrical/Magnetic C Other | Types for Selected Step Symmetry/Antisymmetry/Encastre Displacement/Rotation Connector displacement Secondary base |
| Continue | Cancel |

Figure 11.47. How to create boundary conditions for Frequency calculation step (continuation)



Figure 11.48. How to create boundary conditions for Frequency calculation step (continuation)

| 🔶 Edit Bo | undary Condition | × | |
|--------------------------------------|----------------------|---|--|
| Name: B | C-1 | | |
| Type: D | isplacement/Rotation | | |
| Step: F | requency (Frequency) | | |
| Region: P | art-1-1.INode1 | | |
| CSYS: (G | Global) 🔓 🙏 | | |
| 🔽 U1 | | | |
| 🔽 U2 | | | |
| 🔽 U3 | | | |
| | | | |
| 🗖 UR2 | | | |
| 🗖 UR3 | | | |
| | | | |
| | | | |
| | | | |
| Note: The displacement value will be | | | |
| maintained in subsequent steps. | | | |
| | OK Cancel | | |

Figure 11.49. How to create boundary conditions for Frequency calculation step (continuation)

3. To create calculation step the generation of the superelement click the Create Step button

again (or use double click on the model tree element $\textcircled{I}^{G_{ass}}$ Steps (1), or a menu command Step \rightarrow Create).

In the appeared **Create Step** window, (Figure 11.50) enter the name of the calculation step Substructure generation, then in the drop-down list **Procedure type** select **Linear perturbation**, specify the calculation step **Substructure generation** and click **Continue**.

In the **Edit Step** window on the **Basic** tab (Figure 11.51) in the **Description** column specify the name of the problem being solved as Substructure generation, and in the **Substructure identifier** column you should enter a random number, such as 1. This means that the created superement will have the ID Z1. Set the tab **Evaluate recovery matrix** in position **True** and activate the **Whole model** field.

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| ereate step |
|---|
| Name Substructure generation |
| Insert new step after |
| Initial |
| Frequency |
| |
| |
| |
| |
| Procedure type: Linear perturbation |
| Modal dynamics |
| Random response |
| |
| Response spectrum |
| Response spectrum Static, Linear perturbation |
| Response spectrum Static, Linear perturbation Steady-state dynamics, Direct |
| Response spectrum Static, Linear perturbation Steady-state dynamics, Direct Steady-state dynamics, Modal |
| Response spectrum Static, Linear perturbation Steady-state dynamics, Direct Steady-state dynamics, Modal Steady state dynamics, Subspace |
| Response spectrum Static, Linear perturbation Steady-state dynamics, Direct Steady-state dynamics, Modal Steady-state dynamics, Subspace Substructure generation |

Figure 11.50. Creating the Substructure generation calculation step

| 🗕 Edit Step |
|--|
| Name: Substructure generation |
| Type: Substructure generation |
| Basic Options Damping |
| Description: Substructure generation |
| Substructure identifier: Z 1 |
| Nigeom: Off |
| Recovery Region Image: Evaluate recovery matrix for: |
| Whole model C Region: |
| |
| |
| |
| |
| |
| |
| |
| |
| |
| OK Cancel |

Figure 11.51. Creating calculation parameters of the superelement

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On the **Options** tab of the **Edit Step** window (Figure 11.52) set the **Compute redused mass matrix** and **Specify redained eigenmodes by** checkboxes and select **Mode range**. Then specify the eigenforms, which were used to build the superelement. In this particular case in the figure, for example, it is shown that the eigenforms are used from 1 to 10 with the step 1.

On the **Damping** tab of the **Edit Step** window you don't need to point at anything, click **OK**.

| Name: Step-2 Type: Substructure generation Basic Options Damping Generation Options Compute gravity load vectors Compute reduced mass matrix Compute reduced structural damping matrix Compute reduced viscous damping matrix Evaluate frequency-dependent properties at frequency: Retained Eigenmodes Start End Increment L 1 1 10 1 OK Cancel | 🖶 Edit Step |
|---|---|
| Type: Substructure generation Basic Options Damping Generation Options Compute gravity load vectors Compute reduced mass matrix Compute reduced structural damping matrix Compute reduced structural damping matrix Evaluate frequency-dependent properties at frequency: Retained Eigenmodes Secify retained eigenmodes by: C Mode range C Frequency range Data Start End Increment 1 1 1 10 1 | Name: Step-2 |
| Basic Options Damping Generation Options Compute gravity load vectors Compute reduced mass matrix Compute reduced structural damping matrix Compute reduced viscous damping matrix Compute reduced viscous damping matrix Evaluate frequency-dependent properties at frequency: Retained Eigenmodes ✓ Specify retained eigenmodes by: ⓒ Mode range Frequency range Data Start End I 1 10 I 1 10 | Type: Substructure generation |
| Generation Options Compute gravity load vectors Compute reduced mass matrix Compute reduced structural damping matrix Compute reduced viscous damping matrix Evaluate frequency-dependent properties at frequency: Retained Eigenmodes Specify retained eigenmodes by: Mode range C Frequency range Data Start End Increment 1 1 10 1 | Basic Options Damping |
| Compute gravity load vectors ✓ Compute reduced mass matrix Compute reduced structural damping matrix Compute reduced viscous damping matrix Evaluate frequency-dependent properties at frequency: Retained Eigenmodes ✓ Specify retained eigenmodes by: ⓒ Mode range ○ Frequency range Data I 1 I 1 I 1 I 1 I 1 I 1 I 1 I 1 I 1 I 1 I 1 I 1 I 1 I 1 I I 1 II I III IIIIIIIIIIIIIIIIIIIIIIIIIIII | Generation Options |
| Compute reduced mass matrix Compute reduced structural damping matrix Compute reduced viscous damping matrix Evaluate frequency-dependent properties at frequency: Retained Eigenmodes Specify retained eigenmodes by: • Mode range • Frequency range Data Start End Increment I I I OK Cancel | Compute gravity load vectors |
| Compute reduced structural damping matrix Compute reduced viscous damping matrix Evaluate frequency-dependent properties at frequency: Retained Eigenmodes ✓ Specify retained eigenmodes by: ⓒ Mode range ⓒ Frequency range Data Start End Increment 1 1 1 10 1 OK Cancel | Compute reduced mass matrix |
| Compute reduced viscous damping matrix Evaluate frequency-dependent properties at frequency: Retained Eigenmodes Specify retained eigenmodes by: Mode range Frequency range Data Data Start End Increment 1 1 1 10 1 Cancel | Compute reduced structural damping matrix |
| Evaluate frequency-dependent properties at frequency: Retained Eigenmodes Specify retained eigenmodes by: Mode range Frequency range Data Start End Increment Hode I 1 1 1 1 0K Cancel | Compute reduced viscous damping matrix |
| Retained Eigenmodes Specify retained eigenmodes by: Mode range Frequency range Data Start End Increment I I I OK Cancel | Evaluate frequency-dependent properties at frequency: |
| Specify retained eigenmodes by: Mode range Data Start End Increment I I I OK Cancel | Detained Figenmodes |
| Mode range Frequency range Data Start End Increment I 1 1 10 1 OK Cancel | Specify retained eigenmodes by: |
| Data Start End 1 1 1 1 0K Cancel | Mode range Frequency range |
| Start End Increment 1 1 10 1 | Data |
| | Start End Increment |
| | - Hode Hode |
| OK Cancel | |
| OK | |
| | OK |

Figure 11.52. Creating calculation parameters of the superelement (continuation)

Then set the boundary conditions for the **Substructure generation** calculation step in the interface nodes. To do that in the model tree in the **Substructure generation** section click twice on the item **BCs** (Figure 11.53).

In the appeared window **Create Boundary Condition** choose the category of boundary conditions **Mechanical**, type for selected step **Retained nodal dofs** and click **Continue** (Figure 11.54). Then you must either select the interface nodes with the mouse in the graphics window or use a pre-formed node **Set**. Then click the **Done** button at the bottom of the graphics window (Figure 11.55).

In the appeared window **Edit Boundary Condition** choose the fixed degrees of freedom (Figure 11.56).

Note. The fixed degrees of freedom in the **Edit Boundary Condition** window have to be acceptable for the types of finite elements, used in the model.



Figure 11.53. Setting boundary conditions for Substructure generation calculation step

| 🔶 Create Boundary Co | ondition X |
|-------------------------|--------------------------------|
| Name: BC-2 | |
| Step: Substructure gen | eration 🔽 |
| Procedure: Substructure | generation |
| Category | Types for Selected Step |
| Mechanical | Symmetry/Antisymmetry/Encastre |
| C Fluid | Displacement/Detation |
| C Electrical/Magnetic | Retained nodal dofs |
| C Other | |
| | |
| | |
| | |
| | |
| | |
| Continue | Cancel |

Figure 11.54. Setting boundary conditions for **Substructure generation** calculation step (continuation)



Figure 11.55. Setting boundary conditions for **Substructure generation** calculation step (continuation)

| 🖶 Edit | Boundary Condition |
|---------|---|
| Name: | BC-2 |
| Type: | Retained nodal dofs |
| Step: | Substructure generation (Substructure generation) |
| Region: | Part-1-1.INode1 |
| 🔽 U1 | |
| 🔽 U2 | |
| 🗹 U3 | |
| UR1 | |
| UR2 | |
| UR3 | |
| | OK Cancel |

Figure 11.56. Setting boundary conditions for **Substructure generation** calculation step (continuation)

4. To create an analysis project in the project tree click twice on the **Job** item (Figure 11.57) or right-click and select **Create Job**. Click **Continue** in the appeared window **Create Job** (Figure 11.58).



Figure 11.57. Creating analysis project

An edit job window appears (Figure 11.59). To accept the default parameters click **OK**.

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Figure 11.58. Create Job window

| 🜩 Edit Job | × |
|---|---|
| Name: Job-1 | |
| Model: Model-1 | |
| Analysis product: Abaqus/Standard | |
| Description: | |
| Submission General Memory Parallelization Precision | |
| _ Job Type | |
| • Full analysis | |
| C Recover (Explicit) | |
| C Restart | |
| Run Mode | |
| Background C Queue: | |
| ⊂ Submit Time | |
| © Immediately | |
| C Wait: hrs. min. | |
| C At: | |
| OK | |

Figure 11.59. Edit Job window

Right-click on **Job** in the model tree and choose the item **Manager** in the context menu (Figure 11.60).

In the appeared **Job Manager** window click the **Write Input** (Figure 11.61) button. In the working directory of the **ABAQUS** program a file will be created with the name of the project for analyzing (in our example it is Job-1) and the inp extension. To change the current working directory of the **ABAQUS** program use the menu command **File** \rightarrow **Set Work Directory** (Figure 11.62).



Figure 11.60. Starting Job Manager

| 📥 Job Manager | | | | | × |
|---------------|---------------|------|---------------|--------|-------------|
| Name | Mode | | Туре | Status | Write Input |
| Job-1 | Model- | 1 | Full Analysis | None | Data Check |
| | | | | | Submit |
| | | | | | Continue |
| | | | | | Monitor |
| | | | | | Results |
| | | | | | Kill |
| , Crusta | E-4 14 | Cany | Denema | Delete | Dismiss |
| Create | Edit | Copy | Rename | Delete | Dismiss |

Figure 11.61. Job Manager window



Figure 11.62. How to change the current work directory in the ABAQUS program

to the current work directory.

Cancel

OK

Then you need to change the generated *. inp file by opening it in a text editor.

To output eigenforms, nodes and elements at the stage of description of the parameters of calculation of the natural frequencies before the last line *END STEP you need to enter the command of the matrix output in the output file *.fil.

```
** STEP: Frequency
```

```
*ELEMENT MATRIX OUTPUT, MASS=YES, ELSET=Part-1-1___PickedSet2
```

Macro Manager...

Abaqus PDE... 1 D:/MyTest0.cae 2 D:/MyTest.cae

3 D:/.../MyTest/MyTest.cae 4 C:/1213132/Test4.cae

Ctrl+P

Ctrl+Q

Print...

E<u>x</u>it

***NODE FILE** U

```
*END STEP
```

At the end of the file before the last line (*End Step) you need to enter the command to output matrices of mass and stiffness in the output file *.fil. The last lines in the Job-1.inp file should look like this:

** STEP: Superelement

```
. . .
. . .
. . .
```

.

| Universal Mech | anism 9 | | 11-6 | 3 Part 11. Sir | nulation of flex | ible bodies |
|----------------------|---|--|---|---|---|---|
| *SUBSTRU | JCTURE | MATRIX | OUTPUT, | STIFFNESS=YES, | MAS=YES, | RECOV- |
| ERY=YES *END STEI | P | | | | | |
| Note. | The ELSE includes a The name is already generating specify a s assembly Elset, els l, 60, 1 Therefore the ELSE tion of fin | ET parameter Il the FE mo of the samp present beca g the finite el set of all crea is Part-1-1 et=Part-1-1 in the outpu T parameter ite elements | takes the va dels (in the e le that includ use the prog lements. Belo ated FE mode _PickedSet2. _PickedSet2 t matrixes co on the value | lue corresponding to example above it is Pa les all the finite eleme ram creates and uses ow are the lines from els from 1 to 60 with , generate mmand in the output which is used in You | the name of the art-1-1Pickec ents in the file J it, for example, the file Job-1.in step 1, the nam file replace the ur *.inp file in th | e set which ISet2). ob-1.inp. when np., which e of the value of ne genera- |

After all changes save the *.inp file.

To run the *.inp task file for the calculation in the job manager, click **Create** in the dialog box **Create Job** that appears, select *.inp file and click **Continue** (Figure 11.63). Edit job window will appear (Figure 11.59). Click **OK** to accept all default settings.

| - Create Job X |
|----------------------|
| Name: Job-1-1 |
| Source: Input file 💌 |
| Input file: 📑 |
| C:\Temp\Job-1.inp |
| |
| |
| |
| Continue Cancel |

Figure 11.63. Create job window

Make the project, based on the modified *.inp file, active and run the task for simulation by clicking **Submit** in the Job Manager (Figure 11.64). **Abaqus** in the working process allows monitoring when carrying out the calculation. To do this, click the **Monitor** button in Job Manager. In the appeared dialog window at the **Errors** and **Warnings** tabs you can view the critical errors and warnings that may occur during the calculation.

| 📥 Job Manag | jer | | | × |
|-------------|----------------|---------------|--------|-------------|
| Name | Model | Туре | Status | Write Input |
| Job-1 | Model-1 | Full Analysis | None | Data Check |
| Job-1-1 | File:Job-1.inp | Full Analysis | None | Submit |
| | | | | Continue |
| | | | | Monitor |
| | | | | Results |
| | | | | Kill |
| Create | Edit Copy | Rename | Delete | Dismiss |

Figure 11.64. Calculation running

Upon successful completion of the calculation in the working directory *.fil file will be created which contains the data to import in the **UM**.

11.2.4.4. Data exchange with ABAQUS

Run the converter **ABAQUS_UM.EXE** to create a file input.fum. Select the *.fil file in the appropriate directory and specify the directory in which to save the file input.fum. The purpose of all fields is clear by their names.

| 👑 Creating data se | et for simulation of flexible body | × |
|---|--|-----|
| Paths to data Path to file *.fil: | | |
| D:\Model\ModelForU | JM.fil | |
| 🔽 Save to the same | directory | _ |
| Target directory: | | |
| D:\Model | | õ |
| Abaqus 6.10-1 Description Information input Solution name: | Beam | |
| Comment: | Comment | -11 |
| Date and time Data file System Denter | Date (dd:mm:yyyy): 19.04.2017 Time (hh.mm.ss): 19:17:18 | |
| Create C | Close | |

Figure 11.65. ABAQUS_UM.exe window

In the corresponding dialog box fields you can set the solution name, the comment and the date of calculation. These data are attributes of the **UM** model which are being written to the input.fum file.

Use the **Create** button to perform the data conversion. If it was successfully, the file input.fum will be created in the directory specified in the **Target directory**. Further work with this file is described below in Sect. 11.3 "Wizard of flexible subsystems", p. 11-75.

11.2.5. Some features related to preparing FE models

Let us consider several features that should be taken into account during preparing the finite element models of the flexible bodies.

11.2.5.1. Selection of the interface nodes

The following rules should be taken into account for choosing interface nodes.

1. Interface node should be chosen so as to prevent motion of the flexible subsystem as a rigid body during calculation of static modes. Otherwise the model will be mathematically incorrect and cannot be described with the help of Craig-Bampton approach. Figure 11.66 illustrates incorrect (a) and correct (b) sets of the interface nodes.



(b) Correct set of interface nodes

Figure 11.66. Interface nodes. Positions of interface nodes are marked

Both models consist of 8-node solid elements that have 3 translational degrees of freedom in each node. In **ANSYS** the correspondent type of the finite elements is named as **SOLID45**, and in **NASTRAN**² it is named as **HEXA**.

Two interface nodes in Figure 11.66a do not provide immobility of the model as rigid body during calculation of static nodes for lateral displacements along x or z axes. For example, lateral

² Here and below **NASTRAN** means both supported **MSC.NASTRAN** and **NX NASTRAN**

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displacement of node 2 along *x*-axis the flexible body can rotate around *z*-axis. There are no rotational degrees of freedom in the nodes, so fixing the node 1 does not prevent such a rotation.

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Selection of four interface nodes for a plate in Figure 11.66b allows correctly calculating all static modes.

2. All applied forces, besides contact ones, can be applied in UM at the nodes of FE mesh only. To increase the simulation accuracy it is recommended to select all nodes, where any external force is applied to, as interface nodes. Influence of the applied force on the state of the flexible body directly depends on the presence of the correspondent degrees of freedom in the node. Let us consider the model that is shown in Figure 11.67. A plate consists of solid finite elements and interacts with the support via four linear force elements that are attached at the interface nodes. Lateral or longitudinal displacements of the plate lead to non-zero torques in the force element. Absence of the rotational degrees of freedom in the nodes of FE-mesh leads to ignoring arisen torque components during simulation. In other words, angular stiffness of that springs does not influence on simulation results. So the model will be *physically incorrect* if a real or designed prototype undergoes rather big torques. To simulate such a model correctly it needs to add some additional components into FE-model to provide 6 d.o.f. in each interface node. It will be considered in details below.



Figure 11.67. Sample of UM model with flexible subsystem

- 3. All that is written above about force elements is also directly related to reaction forces in joints. For example, if one fixes the plate in Figure 11.67 in two interface nodes at its corners, the plate will freely rotate around the axis that connects both nodes. In such a model each node can be considered as a spherical joint.
- 4. In the reality, any force that acts on the flexible body is transmitted via some area around the ideal attachment point. It means that it would be more realistic model if the force is distributed among several neighboring nodes in comparison with concentrated force application.
- 5. If the interface node does not have 6 d.o.f., it normally means that constraint equations cannot be generated correctly or even cannot be generated at all.

6. Selection of closely situated nodes as interface ones leads to high frequencies in the final solution.

Let us consider some steps that will help us to provide 6 d.o.f. in the interface nodes and to distribute a force via some area.

1. Adding mass point and constraints.

Six degrees of freedom is introduced with the help of a mass point finite element with non zero moments of inertia. It is **MASS21** element in **ANSYS** (keyopt(3)=0) and **CONM2** in **NAS-TRAN**.

In the **ABAQUS** program to generate the nodal mass you can use the command in the main menu **Special** \rightarrow **Inertia** \rightarrow **Create** of the **Property** module (Figure 11.68). In the appeared **Create Inertia** window select the type **Point Mass/Inertia**, click **Continue**, select using the mouse in the graphics window the points, in which the nodal masses will be, or select a set of nodes, which contains nodes in which the nodal masses will be. Then in the appeared **Edit Inertia** window (Figure 11.69) specify the inertia parameters of the nodal mass and click **OK**.

| + Create Inertia X |
|--------------------|
| Name: Inertia-1 |
| Туре |
| Point mass/inertia |
| Nonstructural mass |
| Heat capacitance |
| |
| |
| |
| |
| Continue Cancel |

Figure 11.68. Creating nodal mass in ABAQUS

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|-----------------------|-------|--|
| | | |

| 🜩 Edit Inertia | × |
|---|---|
| Name: Inertia-1 | |
| Type: Point Mass/Inertia | |
| Region: RReg1 | |
| Magnitude Damping | |
| Mass Isotropic: | |
| C Anisotropic: M11: M22: M33; | 1 |
| Rotary Inertia | |
| I11: | |
| I22: I33: | |
| CSYS: (Global) 📐 🙏 | |
| Note: Values will be applied per point. | |
| OK Cancel | |

Figure 11.69. Edit Inertia window

Such a mass point should have very small inertia parameters relatively to inertia of the whole flexible body. After adding the mass point element to the FE-mesh, angular degrees of freedom in the mass point are not connected with the rest degrees of freedom of the flexible body. In order to interconnect angular degrees of freedom with the translational ones the constraint equations should be added to the model.

ANSYS

Use the following menu command Preprocessor > Coupling/Ceqn > Rigid Region or command CERIG, MASTER, SLAVE, UXYZ,

where **MASTER** is the number of the interface node, **SLAVE** is the node that degrees of freedom are eliminated, **UXYZ** means that all translational degrees of freedom are eliminated. Use **SLAVE=ALL** to eliminate degrees of freedom for all selected nodes. One can also use **CE** command to create constraint equations. Using the constraint equations are fully described in ANSYS user's manual.

ABAQUS

In the **ABAQUS** program it is possible to use the **Constraints** button from the **Interaction** module. When you click **Create Constraint**, dialog window **Create Constraint** appears (Figure 11.70) in which you have to select the **MPC Constraint** type and click **Continue**. Then you must select an interface node or set of nodes, including the interface node, and then select the dependent nodes or set of nodes, including the dependent nodes. Finally, the **Edit Constraint** window (Figure 11.71) should appear in which you have to choose a **MPC Type** equal to **Beam** and click **OK**.



Figure 11.70. Create Constraint dialog window

| 🖶 Edit Constraint | × |
|-----------------------------|---|
| Name: Constraint-3 | |
| Type: MPC Constraint | |
| Control point: Part-1-1.In2 | |
| Slave nodes: Part-1-1.RReg1 | |
| MPC Type: Beam | |
| CSYS (Global) 🔓 🙏 | |
| OK Cancel | |

Figure 11.71. Edit Constraint dialog window

NASTRAN

Constraint equations in NASTRAN are introduced by RBE2 element

RBE2 EID GN CM GM1 GM2 GM3 ...,

where **EID** is the element number, **GN** is the number of node with independent degrees of freedom, **CM** are numbers of eliminating degrees of freedom (1 to 6 without spaces), **GMi** are numbers of nodes whose degrees of freedom are eliminating. For example, the following line in NASTRAN

RBE21636212345661103185introduces constraints equations with number 163, 62 is the number of the independent node,

with which nodes 61, 103, 185 are rigidly connected.

To add such an element in MSC.PATRAN one can click **Elements** button in the tool panel, see Figure 11.72. Use the following parameters in the dialog window:

Action: Create Object: MPC (Multipoint Constraints) Type: RBE2

| : | : 0 | × |
|---------------------------|---|---|
| Action: | Create 🔻 | - |
| Object: | MPC▼ | |
| Туре: | RBE2▼ | |
| Analysis Code Type: | Preferences: : MSC.Nastran Structural | |
| MPCID | | |
| 3 | | |
| Thermal | Expansion Coefficient | |
| | | |
| | Define Terms | |
| | | |

Figure 11.72. Constraints in MSC.PATRAN

Click **Define Terms...** to define constrained nodes. Hereby the rigid region with 6 d.o.f. is created.

Let us consider one more case of using constraint equations for simulation of the crank-and-rod mechanism (Figure 11.73) with a flexible rod (Figure 11.74).



Figure 11.73. Crank-and-rod mechanism with a flexible rod



Figure 11.74. FE-mesh of the rod

Two interface nodes should be defined for the rod. The first interface node should be placed in the center of the cross section at the end where the rod connects the slider, Figure 11.75. The second interface node should be placed on the rotation axis in the center of the circular hole at another end of the rod, Figure 11.76.

1. Adding the mass point and constraint equations

As it already described above, let us add the mass point in the first interface node and then add constraint equations to create a rigid region that involves all nodes that lie at the end of the rod, Figure 11.75.



Figure 11.75. Constraint equations at the end of the rod

Then the following steps should be done at the other end of the rod, Figure 11.76:

- add the node at the rotation axis;
- add the mass point at the rotation axis;
- add constraint equations between the central node and all nodes at the inner cylindrical surface.



Figure 11.76. Constraint equations at the circular hole

2. Adding beam elements.

There is an alternative approach to correctly introduce interface nodes for the rod. This approach assumes creating beam elements to introduce 6 d.o.f. in the interface node and transfer the applied force though several nodes. In ANSYS one can use, for example, elements of BEAM4 type.
It is recommended that beams should be of rather small mass and rather high stiffness. Otherwise eigenmodes and frequencies might be changed. Required beam parameters are achieved by using special characteristics of material and the cross section.

If you use beam elements you do not need to create a mass point in the interface node since every node of a beam element has 6 d.o.f.

Using beam elements are shown in Figure 11.77, Figure 11.78.



Figure 11.77. Beam elements at the end of the rod



Figure 11.78. Beam elements in the circular hole

11.2.5.2. Normals for shell elements

External FE software computes and saves calculation results including data for calculation of stress and strains to intermediate files and then the specific convertor creates input.fum or input.fss files, see Sect. 11.2.1. "Exporting finite element model from ANSYS", p. 11-9, and Sect. 11.2.2. "Exporting finite element model from MSC.NASTRAN", p. 11-26. Count of stress components in the node is explicitly determined by the type of the finite element. In some cases the count of stress components depends on the program settings. For example, **ANSYS** SHELL63 element has two stress components on the top and bottom surfaces at keyopt(11)=0; the same element has three stress components: on top, bottom and middle surfaces at keyopt(11)=2.

UM calculates nodal stress as a mean stresses among all elements containing the target node. However UM does not control normals to elements. To get correct stress estimation for shell el-

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ements the use should be sure that all shell elements around the inspected node have the same normal direction. In other words, top and bottom surfaces for the shell elements should coincide. It should be checked directly in FE software you use.

Let us consider the following example of calculation of average stresses on the top surface of the plate, Figure 11.79. The plate is developed in **ANSYS** and consists of SHELL63 finite elements. Top surface is defined by a normal direction. Normal to the selected element has (0; 0; -1) components. Whereas normals to other elements have the opposite direction (0; 0; 1). Correct average stress estimation in node 77 supposes calculation of stresses at top surface of elements 1, 2, 3 and bottom surface of the element 3 and vice-versa.



Figure 11.79. On calculation of mean stresses on surfaces of shell elements

The situation considered above is not checked by UM automatically. User should check normal directions at the stage of the model development in external FE software products (ANSYS, MSC.NASTRAN, NX NASTRAN).

You can inverse the normal direction in **ANSYS** using the following menu command *Preprocessor* > *Modeling* > *Move* / *Modify* > *Reverse Normals* > *of Shell Elements or use ENSYM command*.

11.3. Wizard of flexible subsystems

Wizard of flexible subsystems (Figure 11.80) is implemented as a tool within **UM Input** program and is aimed for flexible subsystems data control and transformation. **Wizard** is also can be used for excluding some modes from the final solution as well as for orthonormalization of modes and excluding rigid body modes. Functions of the **wizard** are quite similar to program-convertors **ANSYS_UM** and **NASTRAN_UM**.

Use menu command **UM Input / Tools / Wizard of flexible subsystems** to open the window of the wizard.



Figure 11.80. Wizard of flexible subsystems

11.3.1. Animation window

An animation window of the **wizard of flexible subsystems** is aimed for visualization of the FE-mesh, nodes and elements, as well as animation of flexible modes. Common functions of animation window are discussed in the Sect. 11.3.1. "*Animation window*", p. 11-76. Here we will discuss additional functions of the animation window concerning visualization of the FE-mesh.

Mouse cursors:

 k_{one} node of the FE-mesh;

one-dimensional finite element: beam, link, pipe;

finite element of shell or plate type;

solid finite element.

Status line shows information about current selected node or element.

Additional buttons that affect for FE-mesh visualization:

- full/simplified FE-mesh (features of full/simplified will be discussed later);
- show/hide nodes;
- \otimes show/hide finite elements.

Besides standard buttons animation window has additional positioning buttons:

q zoom in/out;
 ∞, ⊕, rotating around corresponding axis;
 ⊕
 ⇒ ↓↑ shift left/right, up/down.

Use the context menu to hide/show tool panels, see Figure 11.81.



Figure 11.81.

11.3.2. Control panel

Control panel includes four tabs.

- General tab shows general information about the flexible subsystem.
- Position tab let the user a possibility to change the flexible body position and orientation.
- Image tab contains control elements, which are used for definition of graphical representation of the flexible subsystem.
- Solution tab show information about current solution with the help of two descendant tabs:
 - **Modes** tab shows information about calculated static modes and eigenmodes, as well as control elements for excluding some modes and their orthonormalization;
 - **Rigid body** shows inertia parameters of the flexible subsystem as a rigid body.

11.3.2.1. General tab

| Select data file | General Position Image Solution |
|---------------------------------|--|
| Data file: | Data file: |
| D:\simulation\ac4body\input.fum | D:\simulation\ac4body\input.fum |
| | Subsystem information Data prepared: ANSYS9.0 Name of solution: ac4body Header of solution (comment): 13.05.2006, 23:39:37, Car body of ac4. Finite elements beam4, shell63, mass21 are |
| | Nodes: 1273 |
| | Finite elements: 2724 |
| | Degrees of freedom: 7638 |
| | Normal modes: 20 |
| | Static modes: 24 |
| | Normalization: No |
| a) | b) |

Figure 11.82. General tab

When you just started **Wizard of flexible subsystems** it has the only tab "Select data file", see Figure 11.82a. Data file box contains the last loaded file, if the **Wizard** starts at the first time this field is empty. Use the ... button to start the open dialog, see Figure 11.83.

| 🚆 Read FEM model of object | × |
|---------------------------------|--|
| Scan directory: | ac4body 🗾 |
| D:\simulation\ac4body\ 🖻 | Car body of ac4. Finite elements |
| ⊡ 🗁 D:\simulation\ac4body\ | Nodes: 1273 Finite elements: 2724 Degrees of freedom: 7638 Normal modes: 20 Static modes: 24 Computation with lumped mass m Min. natural frequency: 5.22 Max. natural frequency: 13.93 Generalized mass matrix: presen Generalized stiffness matrix: pres |
| D:\simulation\ac4body\input.fum | |
| OK Cancel | |

Figure 11.83.

This dialog has the following features:

- you can load only *.*fum* files in this dialog;
- the right panel shows summary text information about the selected flexible subsystem. After loading the *.*fum* file the **General** tab looks like it is shown in Figure 11.82b.

11.3.2.2. Solution tab

Let us consider basic features of the Solution tab, see Figure 11.84.

| o il p. v. l | | | | |
|----------------------------------|--|--|--|--|
| General Position Image Solution | | | | |
| Data set © Original | | | | |
| C Transformed | | | | |
| Transformations | | | | |
| exclude rigid body modes | | | | |
| Frequency: 0.300 | | | | |
| Transform Save as | | | | |
| Modes Rigid body | | | | |
| 20 normal modes, 24 static modes | | | | |
| Selected normal modes: 18 | | | | |
| Selected static modes: 24 | | | | |
| 🗹 14. normal, 10.883 🔺 | | | | |
| ✓ 15. normal, 11.298 | | | | |
| 🗆 16. normal, 11.505 | | | | |
| 🗌 17. normal, 11.512 | | | | |
| ✓ 18. normal, 11.522 | | | | |
| ✓ 19. normal, 11.550 | | | | |
| 🗹 20. normal, 11.713 | | | | |
| ✓ 21. static | | | | |
| 🗹 22. static | | | | |
| IV 23_static | | | | |
| Animation of modes | | | | |
| | | | | |
| | | | | |
| Animate | | | | |

Figure 11.84.

There are two tabs in the bottom part of the **Solution** tab: **Modes** and **Rigid body**.

- The **Modes** tab includes the following components.
 - Summary text information
 - List of modes. Each list item corresponds to a mode of the flexible subsystem and shows the following information:
 - index of the mode in the set of modes;
 - type of mode: static or eigenmode;
 - eigenvalue for the eigenmode.

Every list item has a check box, which is shown if the mode is included to the transformed set of modes.

The list of modes is filled according to the following rules:

- eigenmodes according their eigenvalues;
- \circ static modes according to the order of their calculation in the FE program (ANSYS).

The list of modes shows the complete set of calculated eigenmodes and static modes and shows the flexible mode in the animation window. Besides that the list of modes gives the user a

possibility to create new reduced set of modes as a subset of already calculated modes. You should turn on the check boxes that correspond to the modes you are intended to add to the new subset of modes.

- The **Animation of modes** group contains the following elements.
- The **Animate** button starts animation of modes.
- Track bars **Amplitude** and **Rate** set the scale factor and the frames per second for animation correspondently.

| Note. | Maximal number of frames per second depends on number of nodes and finite |
|-------|--|
| | elements of the flexible subsystem, computer performances and settings of graph- |
| | ical representation of the flexible subsystem in the Image tab. |

• The **Rigid body** tab (see Figure 11.85) shows information about position of center of gravity, mass and moments of inertia of the flexible subsystem.

| Modes | Rigid body | | | | |
|---------|--------------|--|--|--|--|
| Center | of mass | | | | |
| X: 0.32 | 22 | | | | |
| Y:-0.0 | 17 | | | | |
| Z:0.60 | Z: 0.602 | | | | |
| Inertia | parameters | | | | |
| Mass | 23378.108 | | | | |
| lss : | 54031.22985 | | | | |
| lyy : | 439021.22440 | | | | |
| lzz : | 427103.23096 | | | | |
| lxy : | 1315.55093 | | | | |
| lxz : | -14137.37004 | | | | |
| lyz : | 152.25853 | | | | |
| | | | | | |
| | | | | | |
| | | | | | |

Figure 11.85.

- The **Data set** radio group defines original or transformed data set as a current one. This group is enabled if the transformed data set is not created.
- **Transformations** group is aimed for orthonormalization of selected flexible modes.
 - Click **Transform** to start transformation process. A new set of flexible modes is created, the source flexible modes is not changed. In the case of successful transformation the **Data set** radio group becomes enabled. Set **Data set** to **Transformed** to control the transformed modes visually.
 - The **exclude rigid body modes** flag mostly should be turned on. Turn off the flag when there is no possibility to exclude rigid body modes automatically. In this case you should exclude rigid body modes manually.
 - The minimal frequency that corresponds to rigid body modes is set in the **Frequency** box, see Sect. 11.2.1.2. "*Creating stress and strain sensors*", p. 11-14.
 - The **Save as** button is aimed for saving the orthonormalized set of modes. Input the full path to the subsystem in the save dialog (Figure 11.86).

| Save flexible subsystem data | | |
|------------------------------|----------|--|
| Path to subsystem data | | |
| D:\simulation\ac4body\ | <u>Z</u> | |
| Save | Cancel | |

Figure 11.86.

A new *input.fss* file will be created in the specified directory. To create another data set you should select the **Original** in the **Data set** group and then prepare the new data set.

11.3.2.3. Image tab

This tab is intended for describing the graphical image of the FE-mesh of the flexible subsystem in an animation window, see Figure 11.87.

| General Position Image Solution | | | | |
|--|--|--|--|--|
| Image O simplified O full | | | | |
| Image parameters Draw nodes Draw finite elements Contour | | | | |
| Sizes Node image Beam curve width Single node FE | | | | |
| Color Visual elements Nodes Single node elements Beam elements Shell and plate elements Solid elements Polygons | | | | |
| Diffuse Emissive Specular Ambient | | | | |

Figure 11.87.

• You can choose **simplified** or **full** options in the **Image** group.

In the **full** mode you can see information about each node and element in the status line of the window when selecting them with the help of a mouse.

If you select the **simplified** mode then the flexible subsystem is shown as one graphical element with all nodes of the FE-mesh. Information about nodes and elements under the mouse is not available in this mode. Nodes are not drawn and flexible subsystem has **Polygons** color, see **Color** group. **Simplified** mode is intended for big FE-meshes and helps to significantly increase animation rate.

11.3.2.4. Position tab

With the help of this tab you can change position and orientation of the flexible subsystem relative to basic inertial system of coordinates *SC0*. All these data influence on the representation of a graphical image of flexible subsystem in the animation window.

The next step of creating the hybrid (rigid + flexible bodies) model is describing the interactions of flexible subsystem and other bodies of the model. Use the **UM Input** program for that.

| General | Position Image Solution |
|-------------|-------------------------|
| Shift | |
| ×: | n |
| y: | n |
| z: | n |
| Rotation | |
| | • 0.00000000 |
| | • 0.00000000 |
| | • 0.00000000 |
| -Shift afte | er rotation |
| × | n |
| y: | n |
| z: | n |
| | |

Figure 11.88.

11.4. Adding the flexible subsystem into a hybrid model

11.4.1. Adding the flexible subsystem

Select the **Subsystems** item in the list of elements in the left part of the constructor window and add a new subsystem by the \square button, see Figure 11.89. Choose the **Linear FE subsystem** item from the drop-down list and then select the flexible subsystem (*input.fss*) in the open dialog. After loading the flexible subsystem input a name for the new subsystem.

| SubS1 | |
|----------------------|--|
| Name SubS1 | |
| _ | |
| included | |
| Linear FEM subsystem | |

| | | 1 | iguic | 11.07. |
|---|---|--------|-------|------------|
| | Upen object Scan directory: D:\simulation ⊡ C:\simula ac4bo | tion | B | × |
| | | | | (No image) |
| ļ | D:\simulation\ac | 4body(| | |
| | ОК | Cancel | | |

Figure 11.89



Note. After adding the flexible subsystem a fictitious rigid body and a 6 d.o.f. joint are automatically created. The fictitious body has a name of solution, see **General** tab. The fictitious joint is not included into the list of elements. The fictitious rigid body and joint are introduced into the model for uniform creating joint and force elements between flexible subsystem and the rest part of the mechanical system.

11.4.2. Flexible subsystem inspector

After loading the flexible subsystem its parameters are shown in the inspector window. This window is similar to **Wizard of flexible subsystems**. Let us consider basic distinctions of this window.

11.4.2.1. General tab

The General tab contains some additional boxes, Figure 11.91.

- **Identifier** is used during the programming under UM environment. Syntax rules for identifiers are given in Sect. 3.3.2.3.2.
- Ancestor shows path to the flexible subsystem source data.
- Angles of orientation (sequence of angles) determine orientation of the flexible subsystem.

| X | | | | |
|--|--|--|--|--|
| wheelset1 wheelset2 Car body | | | | |
| Name Carbody | | | | |
| Linear FEM subsystem 💌 | | | | |
| Comments | | | | |
| | | | | |
| General Position Image Soluition | | | | |
| Identifier: CarBody | | | | |
| Ancestor: | | | | |
| D:\simulation\ac4body | | | | |
| Orientation angles: | | | | |
| Cardan (1,2,3) | | | | |
| Information about subsystem | | | | |
| Data prepared: | | | | |
| ANSYS9.0 | | | | |
| Name of solution: | | | | |
| ac4body | | | | |
| Header of solution (comments): | | | | |
| 13.05.2006, 23:39:37, Car body of ac4. | | | | |
| Finite elements beam4, shell63, mass21 | | | | |
| Nodes: 1273 | | | | |
| Finite elements: 2724 | | | | |
| Degrees of freedom: 7638 | | | | |
| Normal modes: 36 | | | | |
| Static modes: 0 | | | | |
| Normalization: M-Norm | | | | |
| | | | | |

Figure 11.91.

11.4.2.2. Position tab

This tab let the user a possibility to determine initial position of the flexible subsystem in the basic inertial frame of reference according to design of mechanical system.

11.4.2.3. Solution tab

This tab is aimed for informational purposes only. Here you cannot change the set of modes, but you can animate all modes in the current solution.

11.4.2.4. Image tab

Using the tool panel buttons in the **UM Input** main window makes sense for **Simplified** image for flexible subsystem only. **Simplified** or **full** image of the flexible subsystem is defined at the **Image** tab, see Figure 11.92, Figure 11.93.



Figure 11.92. Graphical modes in UM Input window. Fragment of the tool panel.

| ****** | | | | ····· . | |
|------------------------|---------------------------|-----------|-----------|--------------------|--|
| Name: Platform | | | | <u>-14 414 -15</u> | |
| Туре | Type Linear FEM subsystem | | | | |
| Comm | ents/Text att | tribute C | | | |
| | | | | | |
| Gener | ral Position | Image | Soluition | Coordinate systems | |
| Imag | e | | | | |
| 🔘 🔘 Si | implified | | Full | | |
| Imag | e parameters | | | | |
| 📃 📃 Dr | aw nodes | | | | |
| ☑ Draw finite elements | | | | | |

Figure 11.93. Image tab of the flexible subsystem (UM Input).

11.4.2.5. Coordinate systems tab

Using this tab the user can create additional frames of reference to transform stresses and strain that are calculated relatively local frame of reference of the flexible subsystem. In fact, the oriented points, which are described in Sect. 11.4.2.5. *"Coordinate systems tab"*, p. 11-86 of the 3rd chapter of UM User's Manual, are created.

Let us consider an example of using the **Coordinate systems** tab. Let us imagine that we need to estimate axial stresses on the inclined beam of a railway bridge, Figure 11.94. Longitudinal axis of the inclined beam coincides with no one axis of the local frame of reference of the flexible subsystems.

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Let us create an additional Coordinate system relative to the local frame of reference of the

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flexible subsystems. Let us orient x-axis along to the longitudinal axis of the beam. Click button to create new **coordinate system**. Position of the origin and orientation of the new coordinate system are expressed in the local frame of reference of the flexible subsystem in the fields of the dialog window, Figure 11.95.

There is an alternative way to define a new **coordinate system**. Click **Get by 3 points** button and step by step visually define the node for origin, another node to determine the Xdirection and the third node to determine XY-plane, Figure 11.96. The process of selecting the nodes of the FE-mesh is shown in Figure 11.96a and the results are shown in Figure 11.96b. Xaxis is depicted along longitudinal beam axis.

As soon as the new **Coordinate system** is defined one can express stresses and strains in the nodes of the inclined beam in projection on newly defined **coordinate system**. To create new variable use **UM Simulation / Tools / Wizard of variables**.



Figure 11.94. Fragment of the railway bridge with inclined beam

| Name: | Bridge | | | <u>-1+ +++ -1-</u> |
|-------------|----------------------|----------------|-------------------|--------------------|
| Туре | tinear FEM sub | system | | • |
| Comm | ents/Text attribute | с | | |
| | | | | |
| Gene | al Position Imag | e Soluition | Coordina | ate systems |
| Vc | oordinate systems a | re visible | | |
| Con | diante quatem for th | o indinod bo | | |
| | unate system for u | e inclined be | | |
| - <u>1-</u> | | | | |
| Name | : Coordinate system | for the inclin | ed beam | |
| Coo | rdinates | | | |
| 3.24 | C 2.9 |) | ^C 1.78 | C |
| Orie | ntation | | | |
| X | -180.000000 | 00 | | 1 |
| Y | ▼ 53.80000000 | | | 1/1 |
| 7 | • 0.0000000 | | | • |
| | | | | ∠ • |

Figure 11.95. Coordinate systems tab



Figure 11.96. Creating coordinate system by three points

11.4.3. Features of adding joints and forces

After adding the new flexible subsystem it is necessary to describe attached joints and force elements. Basics of creating joints and force elements are given in the Sect. 11.4.3. "Features of adding joints and forces", p. 11-88.

The following types of joints are supported for the flexible subsystems:

- rotational;
- translational;
- 6 degrees of freedom;

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- generalized;
- rod.

The following types of force elements are supported:

- bipolar forces of all kinds;
- linear force elements;
- contact forces **Points-Plane** type (with some restrictions, see below) and **Flexible body Flexible body** type.

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• T-Forces.

Below we will consider some basic distinctions.

• When you describe a joint or a force element for the flexible subsystem you should select a fictitious rigid body that has the solution name as one of the body in the joint/force, see Figure 11.97.

| Name: | SpringFL | | | | * * * * * * * * * | <u>_+</u> + +: | \$ <u>-1-</u> |
|------------|------------|-------------|--------|----------|-------------------|--------------------|---------------|
| Comm | nents/Text | t attribute | C | | | | _ |
| Body 1: | 1 | | i | Body2: | | | |
| Base0 | | | - | Platforr | n.Platfor | m | - |
| Type: | Viscou | s-elastic | | a - 🗳 | Vibrost | and_Dura ternal | ability |
| GO: [| Spring | | | | - 🖹 Bas | se0 | |
| Positi | on Parar | neters | | 4 | - 🗳 Pla | tform | |
| | | | | 1 | | Platform | n vr |
| | compute fo | r the 2nd | body | - | 7 B | Body | ~ |
| Au | utomatic o | Flexit | ole b | ody | /₽ | Rotor | |
| Body | 1 Body | Pla | tforr | n | ····· 🗗 | Cover | |
| Syste | m of coord | dinates at | pt. A | | 1 | | |
| h [| BeamLeng | th/2 🖸 -\ | Width! | | | | |
| | | 0.000000 | 00 | | | | 2 |
| | • | 0.000000 | 00 | | | | 1 |
| | • | 0.000000 | 00 | | | | 1 |
| Point | B1 - the e | nd of elem | ent: | | | | |
| 1 2 | BeamLeng | th/2 🖸 -\ | WidthS | helf/2- | C | | С |

Figure 11.97. Selecting flexible bodies

• A joint or a force element can be attached in a node of the FE-mesh only. You should keep in mind this fact during creating FE-mesh of the flexible body and specially create nodes so as it would be a node for each attached joint or force element. If there is no a node in the point where a joint/force should be attached to the flexible body, program will find the near-est node for this joint/force. It might lead to relatively significant inaccuracy of the simulation results.

- Joint point of force attachment point may be selected visually after clicking button. Along with coordinates of the attachment point the body itself will be selected or changed.
- If the flexible body was already selected as one of interacting bodies when clicking the following popup menu appears, Figure 11.98.





• Use Select from the nearest nodes menu item to observe the list of the five nearest nodes to the point that coordinates are given in the files for force element or joint. Each line includes the number of node, its coordinates and the distance (d) to the target point, see Figure 11.99.

| Select node of FE-mesh | | | | | | |
|---|--|--|--|--|--|--|
| List of nodes nearest to point: | | | | | | |
| 1. Node 173 (0.500, -0.250, 0.000), d=0 2. Node 350 (0.500, -0.250, 0.007), d=0.0075 3. Node 176 (0.500, -0.263, 0.000), d=0.0125 4. Node 268 (0.500, -0.237, 0.000), d=0.0125 5. Node 351 (0.500, -0.250, 0.015), d=0.015 | | | | | | |
| | | | | | | |
| OK Cancel | | | | | | |

Figure 11.99. List of nearest nodes

11.4.3.1. Features of defining the contact forces for flexible bodies

A flexible body can interact with other bodies of the model via contact forces of the following two types.

1. **Points-Plane** contact force. Description of this force element is considered in Sect. 3.4.9.3.1 of UM User's Manual. Contact points are described for one body and the contact plane is described for another body. The flexible body can be only the body for assigning contact points only. Contact plane cannot be assigned with the flexible body.

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- Contact force of Flexible body Flexible body type. Mathematical model of the force is based on the point-plane contact model, Sect. 2.4.6.1 of UM User's Manual, and is modified to consider features of flexible bodies. To describe this type of contact force the user only needs to specify flexible bodies.
- 3. Contact points are assigned with the first body that interacts with the second body that is considered as a set of triangular plane elements. The whole surface of the second body is considered automatically. If the finite element face that is lies on the surface is triangular then contact polygon coincide with the face. Otherwise the face of the finite element is divided into several triangular polygon implicitly. At each integration time step each contact point interacts with the only contact polygon. The contact point cannot interact with several contact polygons simultaneously. For each *contact point contact polygon* pair the *point plane* mathematical contact model is used. Contact force acts on the first body at the contact point and is reduce to nodal forces for the second body, Figure 11.101. There are no torque components in the contact.
- Note. Simulation results significantly depend on smoothness of the shape of the FE mesh of the second body. Finite element borders are treated as, in fact, borders of contact planes. The FE-mesh with rather large finite elements may lead to step-wise changing of the contact forces whilst moving the contact point from one finite element to another one. It is recommended to keep the size of finite elements small enough to keep rather smooth contact forces.



Figure 11.100. Contact of two flexible bodies



Figure 11.101. On the algorithm of contact force calculation



Figure 11.102. On transformation of the arbitrary applied force to nodal forces

The algorithm of the reduction of the arbitrary applied force to nodal forces has two stages. At the first stage, force **P** applied at point **K** is reduced to equivalent pair of forces applied at points \mathbf{K}_1 and \mathbf{K}_2 . At the second stage force \mathbf{P}_1 is reduced to \mathbf{P}_{11} and \mathbf{P}_{12} and \mathbf{P}_2 is reduced to \mathbf{P}_{21} and \mathbf{P}_{22} . Forces \mathbf{P}_{12} and \mathbf{P}_{22} are summarized for the triangular elements. The following equation is satisfied:

$$\mathbf{P}_{1}L_{1} = \mathbf{P}_{2}L_{2}, \mathbf{P}_{11}L_{11} = \mathbf{P}_{12}L_{12}, \mathbf{P}_{21}L_{21} = \mathbf{P}_{22}L_{22}.$$

Let us consider a dialog window for setting parameters for Flexible body – Flexible body contact force element.

Parameters tab is the same for all types of contact forces, see Sect. 3.4.8.3.

Geometry tab contains the list of contact nodes of the first body and the flag that allows making the second body invisible whilst selecting nodes on the first one. Selection of nodes window is used for defining the contact nodes, Figure 11.103. Click \square^{4} to add new nodes. Nodes, selected during the current and preceding sessions are marked in different colors, Figure 11.104.

Contact node can be *active* or *inactive*. Turn on/off the correspondent check boxes in **Selec-tion of nodes** window to make nodes active/inactive, Figure 11.103. Inactive nodes do not take part in the contact interaction. Turning off the flag in mechanical sense is equal to removing the

node from the list. This possibility helps the user to change the list of contact nodes relatively quick.

| Selection of nodes | × |
|--|--|
| List of flexible subsystems | Nodes in group: 4 |
| Platform 🔻 | Nodes selected: 3 |
| Search node | List of nodes: I. Node 800 (-0.300, -0.238, 0.000) 2. Node 801 (-0.300, -0.225, 0.000) |
| Node number: 803 n Node coordinates: -0.283 -0.237 0.000 - | S. Node 802 (-0.300, -0.212, 0.000) ✓ 4. Node 803 (-0.283, -0.237, 0.000) |
| Selected node N: 803 X: -0.283 Y: -0.237 Z: 0.000 Search Add Clear Close | |

Figure 11.103. Selection of nodes



Figure 11.104. Selection of contact nodes

Let us consider the interaction of the flexible cube (body1) with the flexible plate (body2), Figure 11.100. Simulation accuracy increases along with increasing the number of contact points on the cube. However, increasing the number of contact points on the cube makes the simulation time longer. Practically there is some minimal number of contact points that can be considered as a practical optimum – increasing the number of contact points does not influence on simulation results significantly.

11.5. Analysis of dynamics of flexible subsystem in model

Practically all tools, which are available in UM for rigid body modeling, support flexible bodies. The working procedure with the **UM Simulation** program is described in <u>Chapter 4</u>. Let us consider simulation features relating to the presence of flexible subsystems in a UM model.

There are several special tools.

- Export of flexible displacements to ANSYS.
- Data preparing for durability analysis with the help of **UM Durability** module. Let us consider the **UM Simulation** tools for working with flexible subsystems.

11.5.1. Special tools

11.5.1.1. Export of flexible displacements to ANSYS

UM uses the modal approach to simulate stress-strain state of the flexible body during simulation of dynamics of mechanical system. Variables created with the help of **Wizard of variables** can represent stresses and strains, as well as, all kinematical performances as time histories in graphical windows.

Since the modal approach is an approximation of the FE analysis – a rather accurate approximation, but approximation anyway – it loses some accuracy. There is an alternative way to estimate stresses and strains of the full FE model directly in **ANSYS**. It might be an additional stage of the applied research that goes after stress and strain analysis in UM or even separate stage of stress and strain analysis of the flexible model without preliminary analysis in UM.

For stress and strain analysis of the full FE scheme in **ANSYS** boundary conditions saved as **UM Simulation** are used. Boundary conditions are saved as *.ald (**ANSYS Load**) files. Term 'Load' in ANSYS has several meaning including nodal displacements, external forces, gravity forces, pressure, temperature, etc. Files *.ald contains nodal displacements of flexible subsystem that is one of supported kinds of loads in ANSYS. The separate line in APDL language is generated for each degree of freedom. The following command

D,863,UZ,0.0001472

sets 0.0001472 displacement in Z direction (UZ component) of node 863. D is APDL *DOF constraint* command.

ANSYS Load files can be generated for one or several time points. The user selects that time points based on preliminary analysis. Generally several time points with the worst load conditions should be considered.

Note. Generation of ANSYS Load file does not need importing stress and strain data from ANSYS. If it is planned to perform stress analysis directly in ANSYS without calculation of stresses in UM, in such a case stress sensors in ANSYS can be avoided.

Steps that should be done to generate ANSYS Load file in UM software are described in Sect. 11.5.3.4. "*Export flexible displacements to ANSYS*", p. 11-105.

Working with *.ald files in ANSYS supposes the following steps.

- 1. Load previously created FE model.
- 2. Delete all existing loads, constraints and boundary conditions. Free of constraints object should be considered.

Note. It is recommended to save FE model in ANSYS as separate *.db file as soon as it is ready, prior to running macro to export it to UM.

- 3. Load *.ald files with the help of File | Read Input from... menu item.
- 4. Run static analysis, for instance, with the help of APDL command ANTYPE,STATIC
- 5. Analyze simulation results.

11.5.1.2. Preparing data for UM Durability

Universal Mechanism has a built in **UM Durability** module for prediction of damage sum accumulation, see 13 chapter of UM User's Manual. An important part of durability analysis is obtaining the time histories of stresses of flexible body. Such data can be prepared with the help of **UM FEM**.

Nodal stresses in I node are calculated according to formula 11.6. (see Sect. 11.1.2. "*Calculation of stresses and strains*", p. 11-6):

$$\mathbf{\sigma}_{i}^{e}=\mathbf{H}_{i}^{e\sigma}\mathbf{w},$$

where modal matrix $\mathbf{H}_{i}^{e\sigma}$ is constant. Therefore time histories of stresses can be computed based on relation $\mathbf{w} = \mathbf{w}(t)$, where column matrix w is equal to number of modal coordinates.

UM FEM allows a user to save time histories of modal coordinates to file. Later on **UM Durability** will be able to recover stresses in flexible body having modal matrix $\mathbf{H}_i^{e\sigma}$ and column matrix w. Modal coordinates are saved to *.*tmc* and *.*imc* files. Files *.tmc (title of modal coordinates) have header information in text format. Header information includes the following issues:

- 1. name of **UM** model;
- 2. name if the flexible subsystem;
- 3. path to *.fss file that describes the flexible subsystem;
- 4. date of *.fss file generation (in a packed form);
- 5. date of *.tmc file generation (in a packed form);
- 6. number of nodes of FE mesh;
- 7. number of finite elements;
- 8. number of modal coordinates.

Let us consider *.tmc file format.

with FEASubSystem;

ObjectName=PlatformCar;

name=Platform;

path=d:\Simulation\PlatformCar\platform_FEA;

PackDateSolution=20061007;

```
PackTimeSolution=155059;
NodesCount=15748;
FECount=15324;
MCCount=88;
```

Files *.imc (integration, modal coordinates) are binary and contain modal coordinates. Each record has the following format:

 $(t_i, w_1, w_2, ..., w_n)$

where t_i is time, $w_1,...,w_n$ are values of modal coordinates at t_i , n is number of modal coordinates. Time step for saving modal coordinates to *.imc is set in **Step size for animation and data** storage in **Object simulation** inspector, see Figure 11.105. The smaller the step size and bigger a number of modal coordinates the bigger the *.imc file size. Recommended step size is in between 0.001...0.02 s.

| Object simulation inspector | | | | | | | | |
|--|---|---------------------|--|-------|--|--|--|--|
| Solver Identifiers Initial of | onditions Object variables XVA Information Tools | | | | | | | |
| Simulation process parameter | Simulation process parameters Solver options Type of coordinates for bodies | | | | | | | |
| Solver Type of solution BDF Null space method (NSM) Park method RK4 Park Parallel Range space method (RSM) | | | | | | | | |
| Simulation time Step size for animation and Error tolerance Delay to real time simula | 50 data storage 0. 1E tion | 000 2 01 0006 | | | | | | |
| Computation of accelera | tions and reactio | forces | | | | | | |
| Multi-thread force compu Number of threads (max=8) | itation 5 | | | | | | | |
| Computation of Jacobian Block-diagonal Jacobian Keep decomposition of iterative matrix | | | | | | | | |
| Integration | Mes | age | | Close | | | | |

Figure 11.105. Step size for modal coordinate storage

Note. No stress sensors are needed for generation of *.imc file. If no stress are expected be directly analyzed, the model of the flexible subsystem may not contain stress sensors. It would make the file size smaller. Such a model would be faster to simulate and requires less RAM. However UM Durability would not be able to recover stresses without data for stress sensors.

| Univ | ersal | Me | char | nism | 9 |
|------|-------|----|------|------|---|
| | | | | | - |

Sometimes it is recommended to export to UM two flexible subsystems. The first one without stress sensors for generation *.imc files, and the second one with stress sensors to recover stresses based on *.imc files later on. All other parameters of flexible models should be the same.

Example.

Let us fulfill durability analyses of the railway flat platform. UM model *FlatCar* is used. Flexible subsystem is named as *Platform*. File *input.fss* is situated at the following folder:

d:\Simulation\FlatCar\platform_FEA.

As it was described above let use prepare two input.fss files: with and without stress sensors.

- 1. Firstly, copy the input.fss without stress sensors to *d:\Simulation\FlatCar\platform_FEA* and generate a number of *.imc files to correctly represent real load conditions of the flat car.
- 2. Secondly, copy input.fss with stress sensors to the same directory

d:\Simulation\FlatCar\platform_FEA and replace the old file. Run durability analysis. It might be practically useful of the flexible model is big enough and has many stress sensors so as it takes too much time every time to handle with rather big model. If the model is rather small one and is comfortable to work with it is recommended to use the only model with all necessary stress sensors.

11.5.2. Object simulation inspector

If a model contains flexible subsystems then the **FEM Subsystems** tab appears on the **Object simulation inspector**. The tab has the **Simulation, Image** and **Solution** tabs, Figure 11.106.

If the model contains more than one flexible subsystem then the list with all subsystems appears. The user can select a subsystem from the list to set its parameters.

11.5.2.1. Simulation tab

The **Simulation** tab contains the following interface elements:

- **Gravity** flag allows switching on/off gravity. It may be necessary when a subsystem does not have large displacement.
- Switch off all flexible modes flag allows modeling a flexible subsystem as a rigid body. In this case the subsystem has only six joint coordinates as a free body. The flag is enabled if the subsystem interacts with the object by means of force elements only.
- **Fix modal coordinates** flag prevents changing modal coordinates during calculation of initial conditions. Let us consider an example. Let us imagine two bodies, one or two of them are flexible. Bodies are interconnected by a rotational joint. To calculate initial conditions of the simulated object the constraint equations are solved. Joint points of two bodies are place in the same position. There are several possible ways to place both points to the same position, including flexible deformation of the flexible body (bodies). To prevent such a situa-

tion you should set zero to all coordinates for the flexible body at **Initial conditions / Coordinates** tab sheet of **Object simulation inspector** and turn on **Fix modal coordinates** flag. After that UM will consider and treat flexible body as rigid one and will solve constraint equations simply moving and rotating the flexible body as rigid one.

• Store values of modal coordinates. It helps you to prepare the ANSYS Load file and fatigue analysis with the help of UM Durability, Sect. 11.5.1.1. "Export of flexible displacements to ANSYS", p. 11-94, Sect. 11.5.1.2. "Preparing data for UM Durability", p. 11-95. To create ANSYS Load file both Memory and File options are possible. Durability analysis needs the modal coordinates to be saved to a file. You can assign the default file name by clicking Ctrl+ENTER or substant button. Default directory is the directory of the flexible subsystem.

| Object simulation inspector | | | | | | | | |
|---|---|------------|------|-------|--|--|--|--|
| Solver | ver Identifiers Initial conditions Object variables | | | | | | | |
| XVA | Information | FEM subsys | tems | Tools | | | | |
| Subsystem: Platform | | | | | | | | |
| General Simulation Image Solution Options Damping | | | | | | | | |
| General Gravity | | | | | | | | |
| Switch off al | Il flexible modes | | | | | | | |
| Fix modal co | nitial conditions oordinates | | | | | | | |
| Storing Store values of modal coordinates Destination | | | | | | | | |
| Memory File | | | | | | | | |
| File: C:\users\public\documents\um software lab\universal mechanism\7\san | | | | | | | | |
| Integratio | n | Message | | Close | | | | |

Figure 11.106. Object simulation inspector

- The **Damping** group determines internal dissipation, choosing the mathematical model of dissipation and parameters of the model. Let us consider the **Type of definition** group:
 - **Linear model** allows setting the dissipation matrix as a sum of mass and stiffness matrices multiplied by ratios. User can set the values of ratios at his or her discretion.

| Solver Identifiers Initial conditions Object variables XVA Information FEM subsystems Tools Subsystem: Platform General Simulation Image Solution Options Damping Internal dissipation Type of definition Inear model Image Options Damping ratio for each mode Internal dissipation Unear model Damping ratio for each mode Linear model Damping ratio for each mode Damping ratio for each mode Image Calculate N Frequency (Hz) N Frequency (Hz) Damping ratio 1 15.1065 0 2 42.0761 0 3 95.7276 0 4 110.19 0 5 127.259 0 | Object simulation inspector | | | | | | | | |
|---|-----------------------------|---|------------------|------------|---------|----------|---------|-------------|----------|
| XVA Information FEM subsystems Tools Subsystem: Platform General Simulation Image Solution Options Damping Damping Internal dissipation Type of definition Image Image Internal dissipation Type of definition Image Damping ratio for each mode Linear model Deac+bM D=aC+bM Image a: 0.001 Image Damping ratio for each mode Image Calculate Image N Frequency (Hz) Damping ratio 1 15.1065 0 2 42.0761 0 3 95.7276 0 4 110.19 0 5 127.259 0 Image Set to all | Solve | Solver Identifiers Initial conditions Object variable | | | | | | t variables | |
| Subsystem: Platform General Simulation Image Solution Options Damping Damping Internal dissipation Type of definition Damping ratio for each mode Linear model D=aC +bM a: 0.001 n b: 0 n Damping ratio for each mode Calculate N Frequency (Hz) Damping ratio 1 15.1065 0 2 42.0761 0 3 95.7276 0 4 110.19 0 5 127.259 0 Linear time N Set to all | XVA | | | Informatio | n | FEM sub: | systems | | Tools |
| General Simulation Image Solution Damping Internal dissipation Type of definition Internal dissipation Damping ratio for each mode Linear model D=aC+bM a: 0.001 N Frequency (Hz) Damping ratio 1 15.1065 0 2 42.0761 0 3 95.7276 0 4 110.19 0 5 127.259 0 * | Subsyster | m: Pl | atform | 1 | | | | | |
| Options Damping Damping Internal dissipation Type of definition Inear model Damping ratio for each mode Linear model D=aC+bM a: 0.001 n b: 0 1 15.1065 0 2 42.0761 0 3 95.7276 0 4 110.19 0 5 127.259 0 * | General | Simula | ation | Image S | olution | | | | |
| Damping Internal dissipation Type of definition Inear model Damping ratio for each mode Linear model D=aC+bM a: 0.001 Damping ratio for each mode Calculate N Frequency (Hz) Damping ratio 1 15.1065 0 2 42.0761 0 3 95.7276 0 4 110.19 0 5 127.259 0 | Options | s Damp | ping | | | | | | |
| ✓ Internal dissipation Type of definition ● Inear model ● Damping ratio for each mode Linear model D=aC+bM a: 0.001 n b: 0 1 15.1065 0 2 42.0761 0 3 95.7276 0 4 110.19 0 5 127.259 0 * | Dampir | ng | | | | | | | |
| Type of definition | 🔽 Int | ernal dis | ssipatio | n | | | | | |
| Damping ratio for each mode Linear model D=aC+bM a: 0.001 Damping ratio for each mode Calculate N Frequency (Hz) Damping ratio 1 15.1065 0 2 42.0761 3 95.7276 0 4 110.19 0 5 127.259 0 * | Type | of defini | tion | | | | | | |
| Linear model D=aC+bM a: 0.001 n b: 0 Damping ratio for each mode Calculate N Frequency (Hz) 1 15.1065 2 42.0761 3 95.7276 4 110.19 5 127.259 0 • | Un 🔘 Un | ear mod | ieli atio for | each mod | - | | | | |
| D=aC+bM a: 0.001 Damping ratio for each mode Calculate N Frequency (Hz) 1 15.1065 2 42.0761 3 95.7276 4 110.19 5 127.259 Calculate | Linear | model | | cacinitio | - | | | | |
| a: 0.001 n b: 0 n Damping ratio for each mode Calculate N Frequency (Hz) Damping ratio 1 15.1065 0 2 42.0761 0 3 95.7276 0 4 110.19 0 5 127.259 0 • • • • • • • • • • • • • • • • • • | D= | aC+bM | | | | | | | |
| Damping ratio for each mode Calculate N Frequency (Hz) 1 15.1065 2 42.0761 3 95.7276 4 110.19 5 127.259 Set to all | a: 0.0 | 001 | | | r | b: 0 | | | n |
| Damping ratio for each mode Calculate N Frequency (Hz) 1 15.1065 2 42.0761 3 95.7276 4 110.19 5 127.259 Set to all | | | | | | | | | |
| Calculate N Frequency (Hz) Damping ratio 1 15.1065 0 2 42.0761 0 3 95.7276 0 4 110.19 0 5 127.259 0 Set to all | Dampi | ng ratio | for ea | ch mode | | | | | |
| N Frequency (Hz) Damping ratio 1 15.1065 0 2 42.0761 0 3 95.7276 0 4 110.19 0 5 127.259 0 ✓ ✓ Set to all | Cal | culate | | | | | | | |
| 1 15.1065 0 2 42.0761 0 3 95.7276 0 4 110.19 0 5 127.259 0 ✓ ✓ ✓ | N | Frequ | uency (| Hz) | | Damping | g ratio | | <u>^</u> |
| 2 42.0761 0 3 95.7276 0 4 110.19 0 5 127.259 0 Set to all | 1 | 15.10 | 065 | | | 0 | | | |
| 3 95.7276 0 4 110.19 0 5 127.259 0 ✓ ✓ | 2 | 42.07 | 761 | | | 0 | | | |
| 4 110.19 0 5 127.259 0 ▼ Set to all | 3 | 95.72 | 276 | | | 0 | | | |
| 5 127.259 0 • • • • • • • • • • • • • • • • • • | 4 | 110.1 | 19 | | | 0 | | | |
| Set to all | 5 | 127.2 | 259 | | | 0 | | | - |
| Set to all | × > | | | | | | | | |
| | Set to all | | | | | | | | |
| Integration Message Close | | | | | | | | | |

11-99

Figure 11.107. Object simulation inspector / FEM Subsystem / Simulation / Damping

• When **Damping ratio for each mode** is checked the dissipation for every mode as a damping ratio, Figure 11.108. The critical damping ratio equal to 1 and separates non-oscillatory motion from oscillatory motion.

The values of damping ratio for the given range of flexible modes can be assigned with the help of the dialog window (Figure 11.109). Use the popup menu to show this dialog. The frequency interval can be set by indices of modes (Figure 11.109a) or by the value of the frequency (Figure 11.109b).

Since the flexible modes of a subsystem are orthonormal, values of damping ratio could be calculated based on the linear damping model. For that it is necessary to click the **Calculate** button on the **Simulation** tab (Figure 11.106). You can firstly set values of coefficients of linear dissipation model **a** and **b** (Figure 11.110) and then to click the **Calculate** button to calculate damping ratios for each mode. Values of damping ratios are available to edit.

To accept the calculated values for the subsystem click the **Apply** button. The **Cancel** button closes the window without changing the model parameters.

| 📆 Damping ratio for each mode | | | | | | |
|-------------------------------|---------------------|---------------|---|--|--|--|
| Linear | model | | | | | |
| a: 0. | 001 ⁿ b: | 0 | n | | | |
| Calculate | | | | | | |
| Ν | Frequency (Hz) | Damping ratio | | | | |
| 1 | 15.1065 | 0.3 | | | | |
| 2 | 42.0761 | 0.3 | | | | |
| 3 | 95.7276 | 0.3 | | | | |
| 4 | 110.19 | 0.3 | | | | |
| 5 | 127.259 | 0.4 | | | | |
| 6 | 160.851 | 0.5 | | | | |
| 7 | 160.963 | 0.6 | | | | |
| 8 | 278.928 | 0.6 | - | | | |
| Ap | Cancel |] | | | | |

Figure 11.108. Damping ratio

| 📆 Damping ratio | | × | 🚻 Damping ratio | | × |
|-----------------------------|------------|---|--------------------------------|------------|---|
| Frequency interval | 🔘 by value | | Frequency interval by index | ø by value | |
| Min. number: | 1 | n | Min. value: | 1 | n |
| Max. number: | 5 | n | Max. value: | 120 | n |
| Damping ratio: | 0.30 | n | Damping ratio: | 0.30 | n |
| Set for all flexible subsys | tems | | Set for all flexible sub | systems | |
| OK Cancel | | | OK Canc | el | |

a)

b)

Figure 11.109. Damping ratio

| 📆 Damping ratio for each mode | | | | | | | | |
|-------------------------------|----------------|------------------|---|--|--|--|--|--|
| Linear D=a | Linear model | | | | | | | |
| a: 0.0 |)1 <u>n</u> b: | 0 | n | | | | | |
| | Calculate | | | | | | | |
| N | Frequency (Hz) | Damping ratio | - | | | | | |
| 1 | 15.1065 | 0.47458414448812 | | | | | | |
| 2 | 42.0761 | 1.32185977864034 | | | | | | |
| 3 | 95.7276 | 3.00737036888088 | | | | | | |
| 4 | 110.19 | 3.4617161284573 | | | | | | |
| 5 | 127.259 | 3.99794912816365 | | | | | | |
| 6 | 160.851 | 5.05327273016699 | - | | | | | |
| Apply Cancel | | | | | | | | |

Figure 11.110. Linear model of damping ratio

11.5.2.2. Image tab

The **Image** tab is identical to the corresponding tabs of **Wizard of flexible subsystems** and data inspector in **UM Input** program and is described in details in Sect. 11.3.2.3. *"Image tab"*, p. 11-82.

11.5.2.3. Solution tab

Solution tab is identical to the corresponding tab of **Object constructor** that is described in details in Sect. 11.3.2.3. *"Image tab"*, p. 11-82.

11.5.3. Variables

You should use the **Wizard of variables** to create new variables to analyze, see Sect. 11.3.2. *"Control panel"*, p. 11-76. Here we will discuss some features, which are connected with simulation of flexible subsystems.

11.5.3.1. Coordinates

In the list of coordinates of the **Wizard of variables** you can see two groups of elements that correspond to flexible subsystem, Figure 11.111. The first group includes six d.o.f. of a flexible subsystem as a free body (coordinates 2.1-2.6) and the second one includes complete set of generalized coordinates of the flexible subsystem (starting with coordinate 2.7).



Figure 11.111. Coordinates of the model

Note. Modal coordinates are dimensionless variables. That is why make sense only comparative analysis of modal coordinates between each other.

11.5.3.2. Linear variables

Please note that kinematical variables (coordinates, velocities and accelerations) are available for nodes of finite-element mesh only. If there is no node in the indicated point then the nearest node will be chosen and the user will have the correspondent message, see Figure 11.112.



Figure 11.112.

11.5.3.3. Stresses and strains

Variables that are used for estimation of stress-strain state of the flexible body are created at **Wizard of variables / FE Sensors** tab sheet, Figure 11.113.

| 🕎 Wizard of variables | | | | | | x | |
|---|------------|--------------------|-------------------|---------------|------------|------------------|---------------------|
| 🛯 🗳 vibrostand_durability | * | Linear F | User | Expression | Identifier | | |
| A 🗳 Platform | | Coordinates | Angular var. | Reaction F | Linear va | | |
| 1. Node 1 (0.500, -0.300, (| | All forces | Joint force | FE Sensors | Solve | Cı | irrently selected |
| 2. Node 2 (0.500, -0.250, (| | Stresses | | _ | | | node (sensor) |
| 500, -0.228, (| | | | | \sim | | |
| List of sensors | | Platform 1 N | ode 1 (0 500 -0 | 300 0.060) | ́г | _ | |
| . Node 6 (0.200, -9.250, (| | -Kind of soluti | one 1 (0.300, -0 | | | Lis | st of stress/strain |
| 🖹 7. Node 7 (0.483, -0.250, (| | Nodal | on | C Flemental | | | components |
| 🖹 8. Node 8 (0.467, -0.250, (| | | | - Elementar | | | - |
| 9. Node 9 (0.450, -0.250, (| | Element group | S: | Com | ponent: | $\leq \parallel$ | |
| I0. Node I0 (0.433, -0.230 I1 Node 11 (0.417 -0.250 | | 1. SHELL63 (1 | 1) | ▼ SX1 | . / . | | |
| 12. Node 12 (0.400, -0.250 | | | | | | | |
| 13. Node 13 (0.383, -0.250 | | Resolved in SC: | Local SC of | subsystem | | • | |
| List of finite element contains the selected | s tl no | nat de | | | | | |
| 18. Node 18 (0.300, -0.250 | | | List of f | rames of refe | rence | | |
| 19. Node 19 (0.283, -0.250 | Ŧ | L | | | | | |
| ۰ III + III | | | | | | | |
| SX1_N_N1_GroupFE1 Component | nt S | X1 of stress. Plat | form. 1. Node 🛫 | u 🐺 🗡 | | | |
| SX1 N N1 Grou | - | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |

Figure 11.113. FE Sensors tab of Wizard of variables

FE Sensors tab sheet contains two subsidiary tabs **Stresses** and **Strains**. Since **Stresses** and **Strains** tab sheets are identical let us consider the **Stresses** tab only.

Note. FE Sensors tab sheet or one of the subsidiary tabs will be invisible if *input.fss* file that describes the flexible subsystem does not contain data for recovering stresses or strains correspondingly. Data export procedure is considered in Sect. 11.2.1.2. "Creating stress and strain sensors", p. 11-14, Sect. 11.2.2.3. "Preparing data in MSC.PATRAN/NASTRAN environment", p. 11-29.

To create a stress or strain variable the user has to go through the following steps.

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- 1. Select the **Stresses** or **Strains** tab sheet. Please note, that the lists of the nodes (sensors) for both tabs generally can be different.
- 2. Select the node (sensor) in the list. If the loaded model has several flexible subsystems, then the tree of nodes includes all of flexible subsystems with their nodes (sensors). If there are many sensors in the model you can use **Search node** tool, Figure 11.114. **Search node** helps you to find a node by its index (number) or by its coordinates in the local frame of reference of the flexible body. Enter node **Index** or **Coordinates**, click **Search** and **Apply** if the interesting node is found.

| | " Searching node of finite-element 💶 💷 🗮 🎫 | | |
|---|--|--|--|
| | Search node | | |
| 🕎 Wizard of variables | ● by index | | |
| ✓ vibrostand_durability ↓ ↓ ✓ Platform Coc ▲ ● 1. Node 1 (0.500, -0.300, (All □ ● 2. Node 2 (0.500, -0.250, (Stre □ ● 3. Node 3 (0.500, -0.288, (Stre □ ● 5. N Search node ₽ ● 6. Node 6 (0.200, -0.250, (► ► | N: 123 0.450 Y: -0.238 Z: 0.060 Selected node N: 123 X: 0.450 Y: -0.238 Z: 0.060 Apply Cancel Search | | |

Figure 11.114. Search node

- 3. Select **Kind of solution: Nodal** or **Elemental**. Nodal stresses and strains are calculated as mean values for all elements that contains the selected node, see Sect. 11.1.2. "*Calculation of stresses and strains*", p. 11-6. If the node belongs to finite elements of different types, the nodal solutions can be calculated for each type of finite element, see **Element groups** list.
- 4. Select the **Component** of the solution. The list of components contains elements of stress tensor, principal stresses and von Mises stresses. Components for the top and bottom surfaces are available for shell elements. Top and bottom surfaces are defined by normal direction. Captions of the stress components correspond to its conventional captions in the FE software product where the model was developed and exported to UM.

| Wizard of variables | | | | —X — |
|-----------------------------------|-----------------|---------------|-------------------|-------------|
| 🗠 🖹 103. Node 103 (0.450, -0.2 🔺 | Linear F | U <u>s</u> er | Expression | Identifier |
| 104. Node 104 (0.433, -0.2 | Coordinates | Angular var | . Reaction F | Linear var. |
| 105. Node 105 (0.417, -0.2 | All forces | Joint force | FE Sensors | Solver |
| 106. Node 106 (0.400, -0.2 | Strange | | | |
| 107. Node 107 (0.383, -0.2 | Stresses | | | |
| 108. Node 108 (0.367, -0.2 | Sensor: | | | |
| 109. Node 109 (0.350, -0.2 | Platform. 123. | Node 123 (0. | 450, -0.238, 0.06 | <u>i0)</u> |
| 110. Node 110 (0.333, -0.2 | Kind of soluti | on | | |
| 🗠 🖹 111. Node 111 (0.317, -0.2 | Nodal | | Elemental | |
| 🖹 112. Node 112 (0.300, -0.2 | | | 0 210110 |] |
| 🖹 113. Node 113 (0.283, -0.2 | Element group | s: | Co | mponent: |
| 114. Node 114 (0.267, -0.2 | 1. SHELL63 (8 | 35,86,81,82) | ▼ S) | (1 🔫 |
| 🖹 115. Node 115 (0.250, -0.2 | | | S | (1 |
| 🖹 116. Node 116 (0.233, -0.2 | Perolved in SC: | | SY SY | 1 |
| 🖹 117. Node 117 (0.217, -0.2 | Resolved in Sc. | LOCALSC | SZ SZ | 1 |
| 🖹 118. Node 118 (0.200, -0.2 | | | S | Y1 (71 |
| 🖹 119. Node 119 (0.200, -0.2 | | | S) | 71 |
| 🖹 120. Node 120 (0.200, -0.2 | | | St | 1 |
| 🖹 121. Node 121 (0.483, -0.2 | | | S2 | |
| 🖹 122. Node 122 (0.467, -0.2 | | | - | |

Figure 11.115. Stress/strain component list

For example, in **ANSYS** stress components are named SX, SY, SZ, SXY, SYZ, SXZ, S1, S2, S3, SEQV, where S1..S3 are principal stresses, SEQV is von Mises stresses. If shell elements are chosen, then component names are complemented by number 1 for the top surface and 2 for the bottom surface, for examples S12 would be a maximal principal stress on the bottom surface and SEQV1 would be von Mises stress on the top surface.

11.5.3.4. Export flexible displacements to ANSYS

Flexible displacements are exported into **ANSYS** software with the help of the dialog window shown in Figure 11.117. Click **s** tool button in the tool panel of **UM Simulation**. If you cannot find the **s** button you probably need to turn on the **Flexible** subsystems menu command, see Figure 11.116.



Figure 11.116. Popup menu of UM Simulation tool panels

To save a flexible displacement for the flexible body the following steps should be done.

- 1. Turn on **Store values of modal coordinates** flag in **Object simulation inspector / FEM Subsystems / Simulation / Options** tab sheet, see Figure 11.106.
- 2. Open **Wizard of variables** and create variables that will be treated as criteria for time point selection for saving load file.
- 3. Copy created variables to a graphical window.
- 4. Run simulation.
- 5. Open **Export of load files for flexible subsystems** dialog window, see Figure 11.117. Copy variables from the graphical windows to **Export of load files / List of variables** group.
- 6. In **Subsystem** drop down lost select the flexible subsystem you are interesting in.
- 7. Select some specific variable in **Export of load files / List of variables** group. Panel **Analysis of variable** shows some variables-related information like name of variable, minimal and maximal values of variable and the correspondent time points. There is also an edit box where the user can input the time what the ANSYS load file should be generated for.
- 8. Select the desired **Criterion** and **File name** and click **Save**. Click Ctrl+Enter keys or subtraction to generate default file name. Default directory for the load file is the directory of the flexible subsystem. Default file name includes flexible subsystem name, variable name and the selected criterion.

| Export of load files for flexible subsystems | | | | | | |
|--|--|------------------------|--|--|--|--|
| Object | vibrostand_durability | | | | | |
| Subsystem: | Platform | Platform 🔹 | | | | |
| List of variables | ist of variables: | | | | | |
| Name | Comment | | | | | |
| SEQV1_N_N10 Component SEQV1 of stress. Platform. 10. Node 10 (0.4 | | | | | | |
| SEQV1_N_N11_ | SEQV1_N_N11 Component SEQV1 of stress. Platform. 11. Node 11 (0.41 | | | | | |
| Analysis of varia | able | | | | | |
| Variable: SEQV1_N_N11_GroupFE24-Component SEQV1 of stress. Time of integration: from 0.0000 to 2.0000 | | | | | | |
| Max. value: | 8.564016875E+05 | t max: 2.00000000E+00 | | | | |
| Min. value: | 5.649571875E+05 | t min: 1.953999996E+00 | | | | |
| Value: | | 0.0 <u>n</u> | | | | |
| Criterion | | | | | | |
| Max | Min | 🔘 Value | | | | |
| File name: | | | | | | |
| /ibrostand_dura | /ibrostand_durability\platform\Platform SEQV1_N_N11_GroupFE24max.ald 👥 🛄 | | | | | |
| Save | | | | | | |

Figure 11.117. Generation of ANSYS Load file

Note. Modal coordinates are calculated for time steps with an interval that is described in Object simulation inspector / Solver / Simulation process parameters / Step size for animation and data storage field, see Figure 11.105. The closest time point to specified by Value field is stored.
 Note. You can select any arbitrary time point simply analyzed plots of variables in graphical windows.

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